

# An elastic interface approach to failure in microcracked materials

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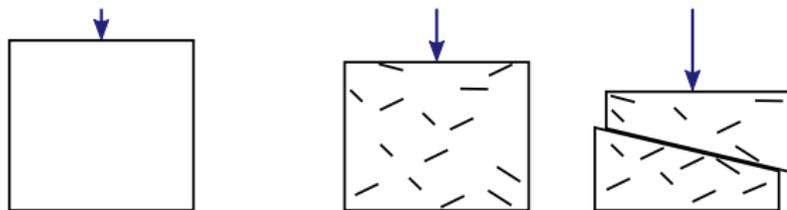
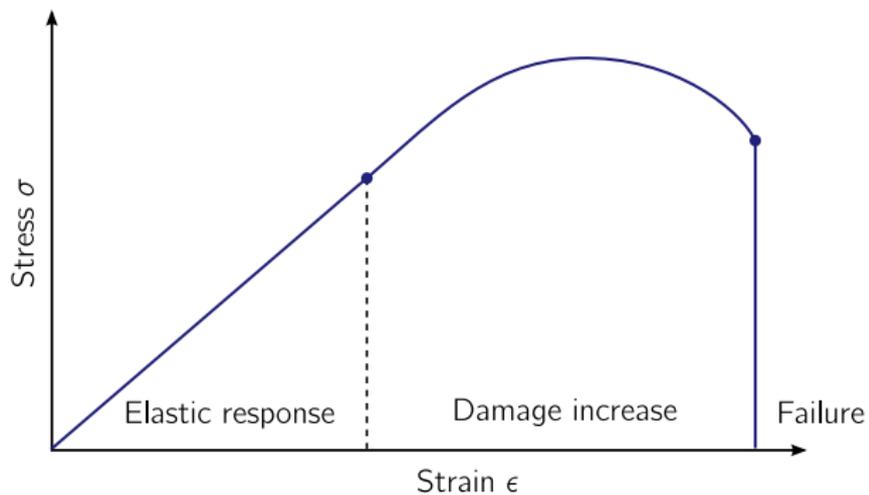
University of Massachusetts, Amherst, USA

→ Gulliver, ESPCI, Paris, France

KITP 2014, October 20<sup>th</sup>

*Thanks: ISCPIF, KECK Foundation*

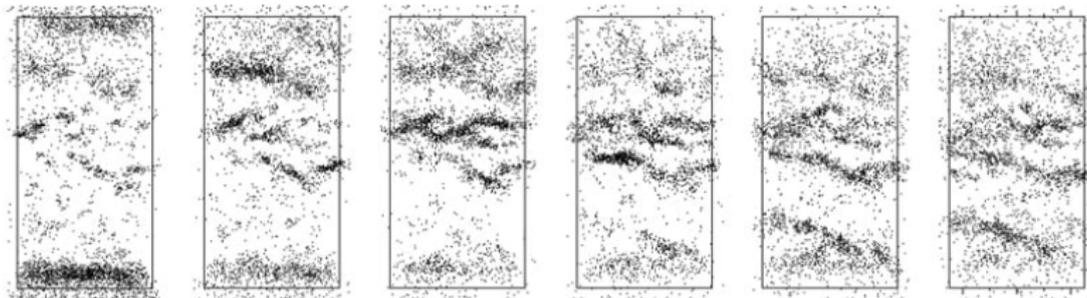
# Phenomenology of damage failure



# Characteristic features

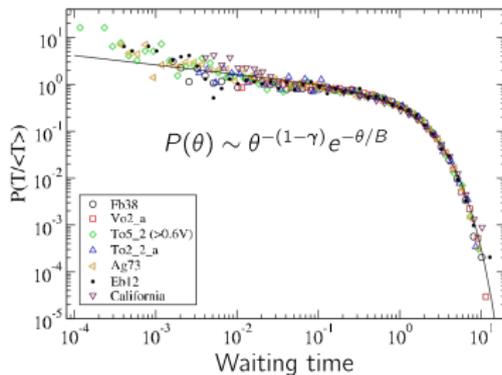
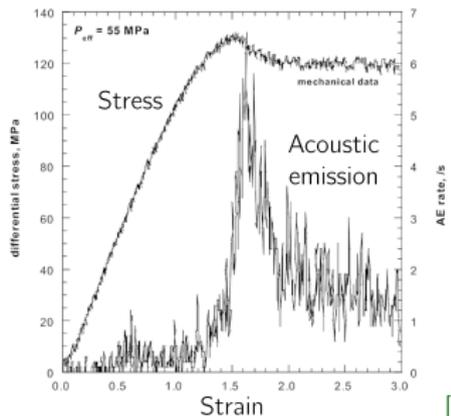
(acoustic emission in compressed sandstone)

## Localization



[Fortin *J. Geophys. Res.* 2006]

## Avalanches



[Baud et al. *J. Struct. Geol.* 2003, Davidsen *PRL* 2007]

# Outline

Introduction to damage models

1d toy model: basic mechanisms

2d realistic model

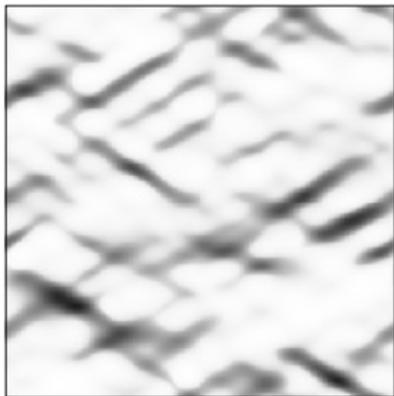
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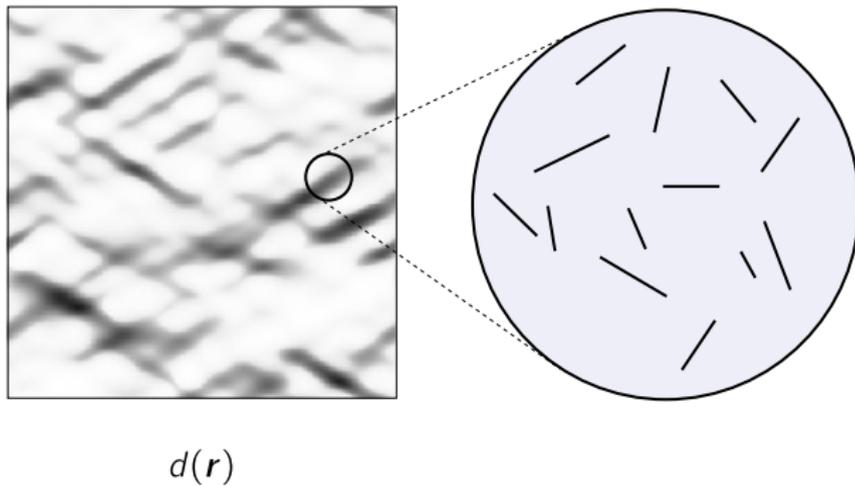
## Definition of damage



$d(\mathbf{r})$

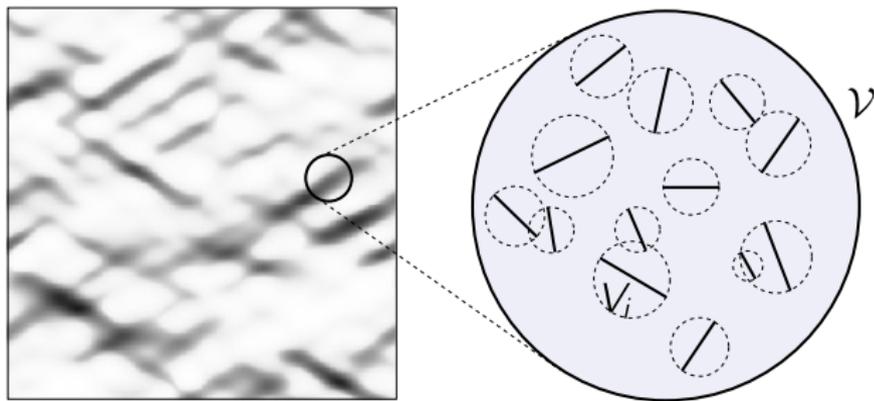
[Ponte-Castañeda, Willis *JMPS* 1995]

## Definition of damage



[Ponte-Castañeda, Willis *JMPS* 1995]

## Definition of damage

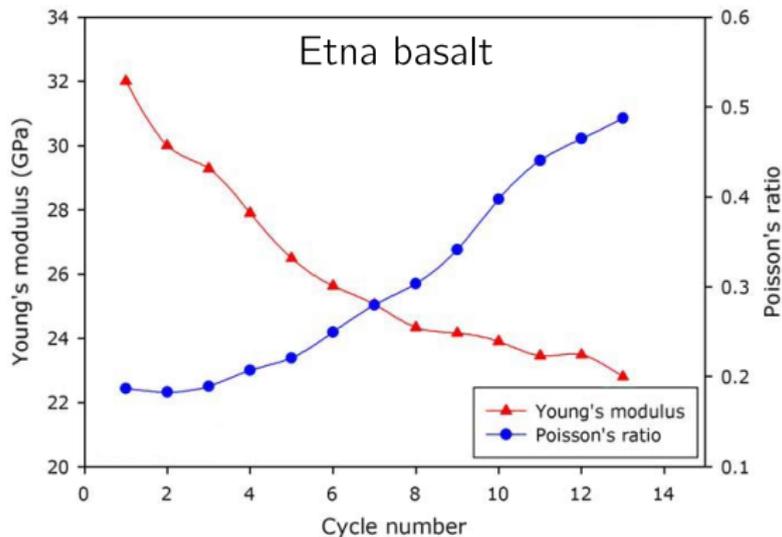


$d(\mathbf{r})$

$$d = \frac{1}{\nu} \sum_i V_i$$

[Ponte-Castañeda, Willis *JMPS* 1995]

## Damage affects the elastic properties



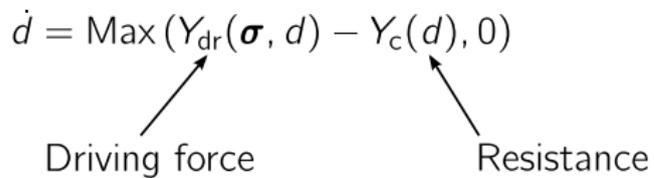
[Heap et al. *Tectonophysics* 2009]

- Simple model:  $E(d) = E_0 \times (1 - d)$ ,  $\nu = \nu_0$ .
- More realistic expressions: Kachanov, Ponte-Castañeda and Willis.

## Damage evolution

$$\dot{d} = \text{Max}(Y_{\text{dr}}(\boldsymbol{\sigma}, d) - Y_{\text{c}}(d), 0)$$

Driving force



Resistance

# Damage evolution

$$\dot{d} = \text{Max}(Y_{\text{dr}}(\boldsymbol{\sigma}, d) - Y_{\text{c}}(d), 0)$$

Damage criterion

Driving force

Resistance

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Energetic

Elastic energy release

$$-\left. \frac{\partial}{\partial d} \left( \frac{\boldsymbol{\sigma} : \boldsymbol{\epsilon}}{2} \right) \right|_{\boldsymbol{\epsilon}}$$

Surface energy

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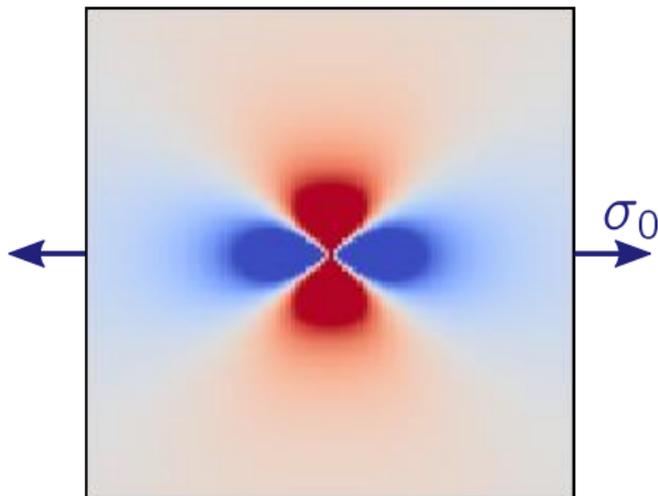
Mohr-Coulomb

Shear stress

Friction

## Heterogeneous elastic properties redistribute the stress

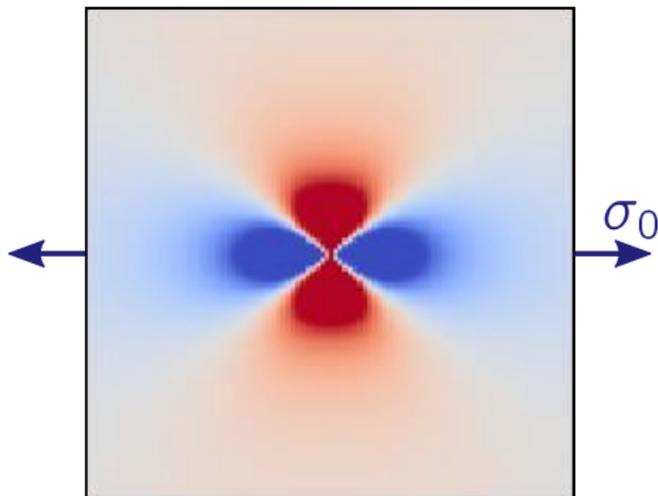
- The stress field around an ellipsoidal inclusion can be found. [Eshelby *PRSL A* 1957]
- General case  $E(\mathbf{r})$ : requires numerical resolution.



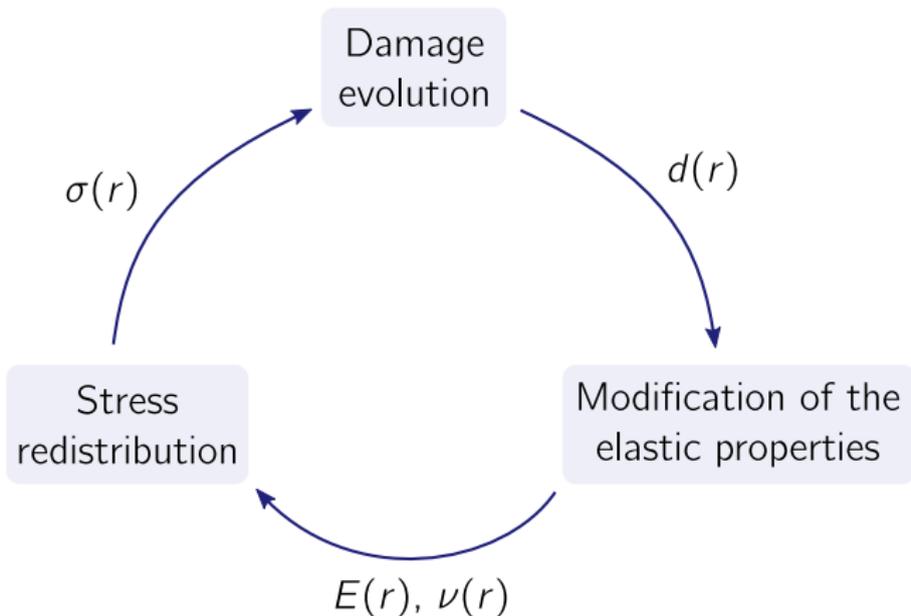
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- General case  $E(\mathbf{r})$ : requires numerical resolution.
- If **heterogeneities are weak**, Eshelby result may be used as a Green function to compute the stress field to the first order in the heterogeneities (**superposition principle**)

$$\boldsymbol{\sigma}(\mathbf{r}) = \boldsymbol{\sigma}_0 + \boldsymbol{\psi}_E * \delta E(\mathbf{r}).$$



## General structure of a damage model



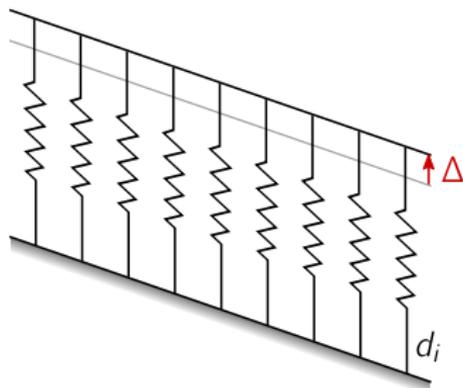
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# 1d model: fiber bundle with interactions



$$E = \frac{\Delta^2}{2} \int k(d(x)) dx + \int \int_0^{d(x)} Y_c(d', x) dd' dx$$

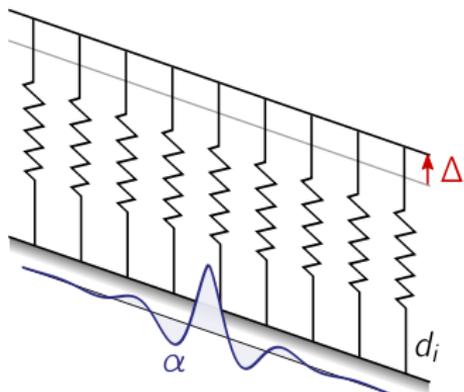
↑ Elastic energy      ↑ Fracture energy

Energetic criterion: damage at  $x$  if  $Y(x) = -\frac{\delta E}{\delta d}(x) \geq 0$ .

Stiffness:

$$k(d) = ad^\zeta - (a+1)d + 1$$

# 1d model: fiber bundle with interactions



$$E = \frac{\Delta^2}{2} \int k(\alpha * d(x)) dx + \int \int_0^{d(x)} Y_c(d', x) dd' dx$$

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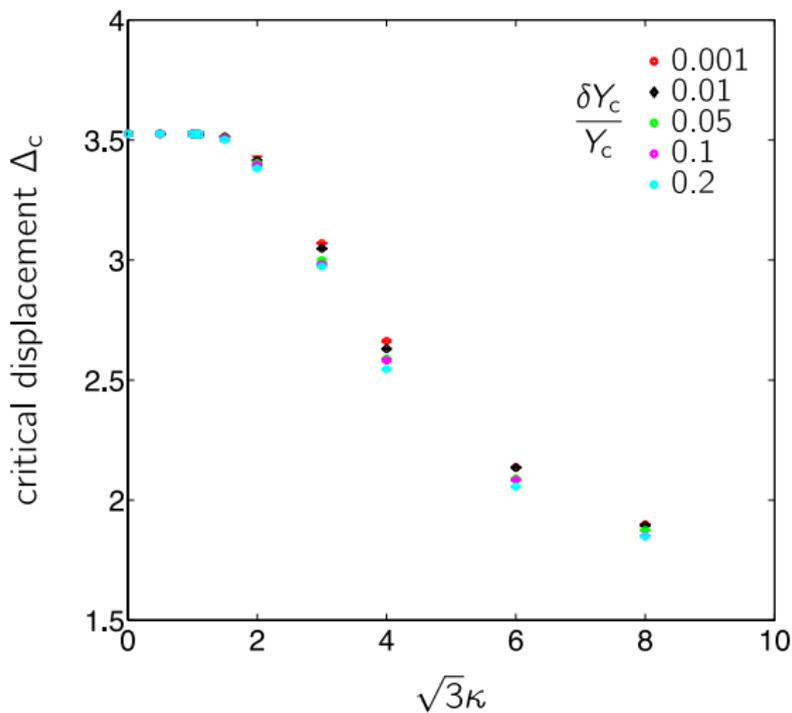
$$k(d) = ad^\zeta - (a+1)d + 1$$

Load sharing:

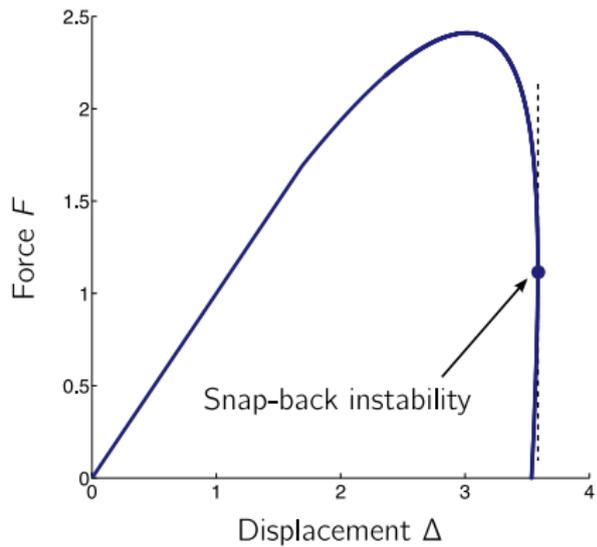
$$\alpha(x) = \exp\left(-\frac{|x|}{l}\right) \cos\left(\frac{\kappa x}{l}\right)$$

## 1d model: numerical simulations

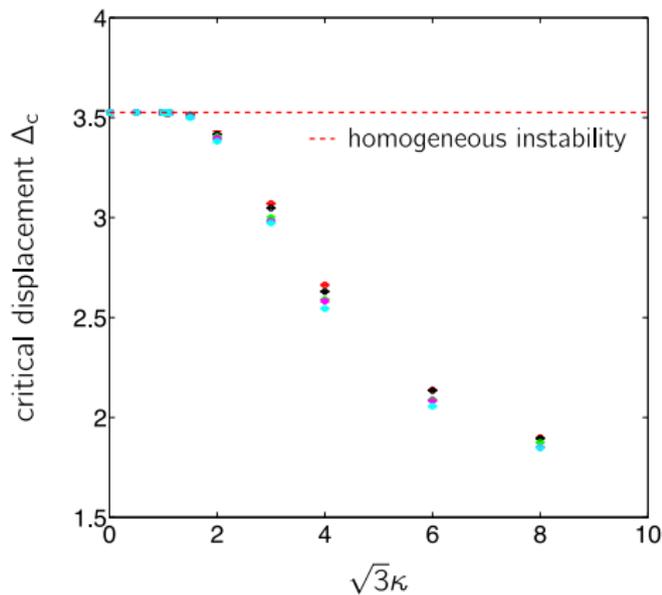
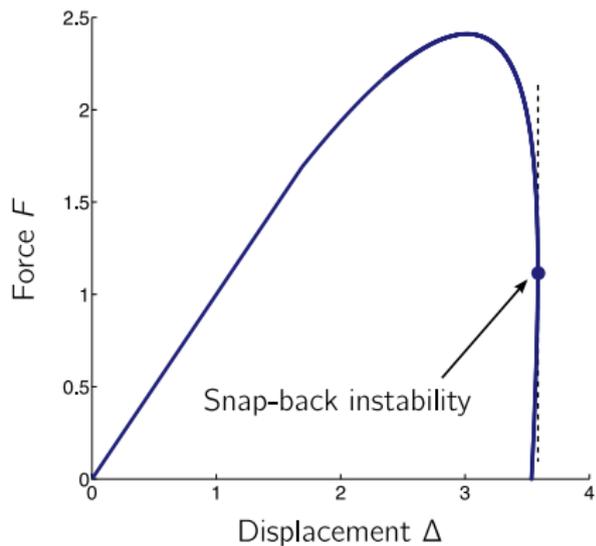
- Load sharing:  $\alpha(x) = \exp\left(-\frac{|x|}{l}\right) \cos\left(\frac{\kappa x}{l}\right)$ .
- Quasistatic evolution.



# 1d model: homogeneous damage evolution



# 1d model: homogeneous damage evolution



$$\alpha(x) = \exp\left(-\frac{|x|}{l}\right) \cos\left(\frac{\kappa x}{l}\right)$$

## 1d model: heterogeneous damage evolution

Expansion of the damage evolution around a homogeneous damage,  $d(x) = \langle d \rangle + \delta d(x)$

$$Y[\Delta, d(x)] = Y(\Delta, \langle d \rangle) + \Psi_{\langle d \rangle} * \delta d(x)$$

$\Psi_{\langle d \rangle}$  values in Fourier space are its eigenvalues:

$$\tilde{\Psi}_{\langle d \rangle}(q) > 0 \Rightarrow \text{the mode } q \text{ is unstable.}$$

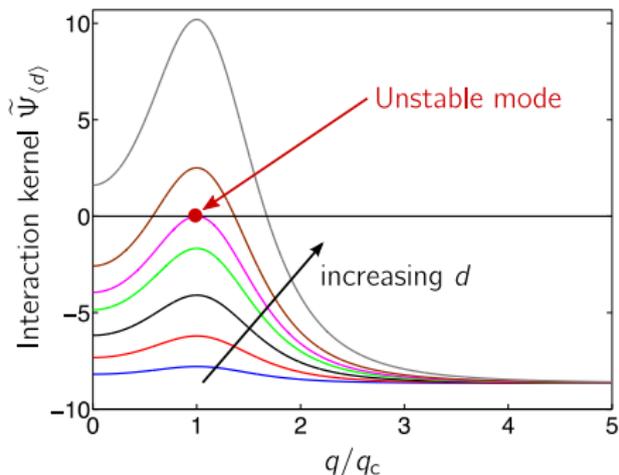
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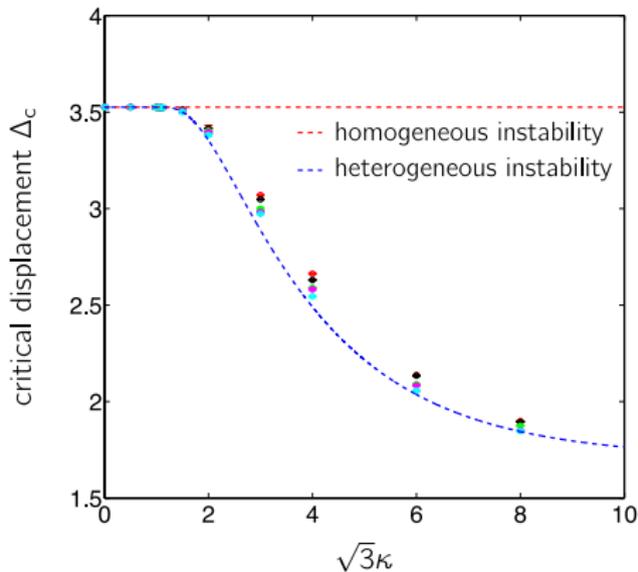
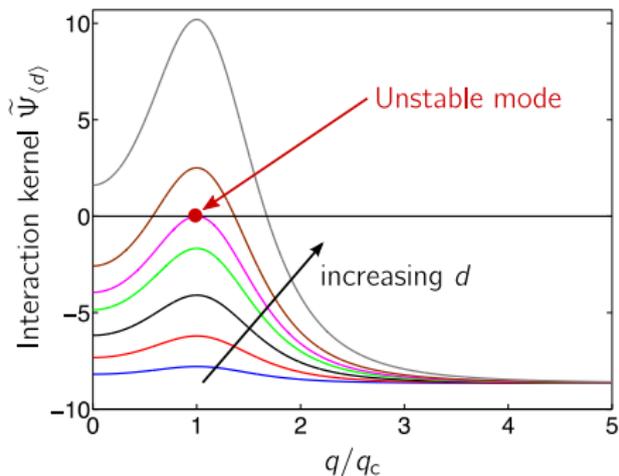
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# 1d model: conclusion

- Initial model: no linear elastic kernel.
- Linear elastic kernel:
  - Obtained by expanding the initial model for a weakly heterogeneous damage  $d(x) = \langle d \rangle + \delta d(x)$ :

$$Y[\Delta, d(x)] = Y(\Delta, \langle d \rangle) + \Psi_{\langle d \rangle} * \delta d(x)$$

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- Stability analysis in Fourier space: sign of  $\tilde{\Psi}_{\langle d \rangle}(q)$ .
- 2 possible cases:
  - $\frac{\partial Y(\Delta, d)}{\partial d} \geq 0$  first: homogeneous instability.
  - $\tilde{\Psi}_{\langle d \rangle}(q_c) \geq 0$  first: **localization** with wavelength  $\lambda_c = 2\pi/q_c$ .
- Different from usual depinning transitions (brittle failure...):
  - Kernel evolves with damage:  $\Psi_{\langle d \rangle}$ .
  - Kernel instability, weak effect of the disorder.

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## 2d model

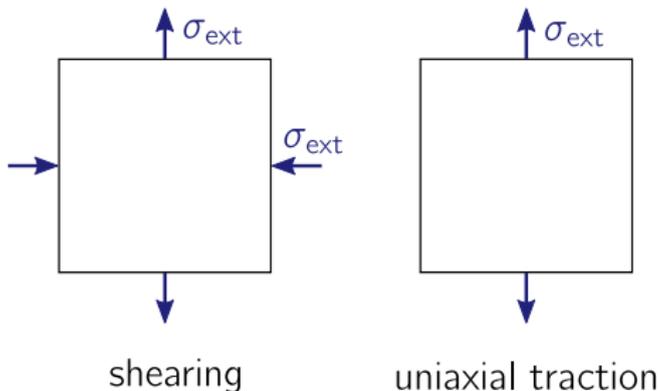
- Energetic criterion for damage evolution (no friction, applies to traction, shear),

$$Y(\boldsymbol{\epsilon}, d) = - \frac{\partial}{\partial d} \left( \frac{\text{Tr}(\boldsymbol{\sigma}\boldsymbol{\epsilon})}{2} \right) \Big|_{\boldsymbol{\epsilon}} - Y_{c0}.$$

- Stress redistribution from continuum mechanics (2d - plane strain),

$$\text{div}(\boldsymbol{\sigma}) = 0,$$

$$\epsilon_{ij,kl} - \epsilon_{jk,li} + \epsilon_{kl,ij} - \epsilon_{li,jk} = 0 \quad \forall i, j, k, l.$$



## 2d model: stress redistribution

Expansion of the driving force for a weakly heterogeneous damage  $d(\mathbf{r}) = \langle d \rangle + \delta d(\mathbf{r})$

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$$\tilde{\Psi}_{\langle d \rangle}(\mathbf{q}) = \frac{a''}{2} \text{Tr}(\boldsymbol{\sigma}^2) + \frac{b''}{2} \text{Tr}(\boldsymbol{\sigma})^2 - \frac{1}{a+b} [a' \text{Tr}(\boldsymbol{\sigma} \mathcal{O}(\mathbf{q})) + b' \text{Tr}(\boldsymbol{\sigma})]^2$$

$$\boldsymbol{\epsilon} = a\boldsymbol{\sigma} + b\text{Tr}(\boldsymbol{\sigma})\mathbf{1}$$

## 2d model: stress redistribution

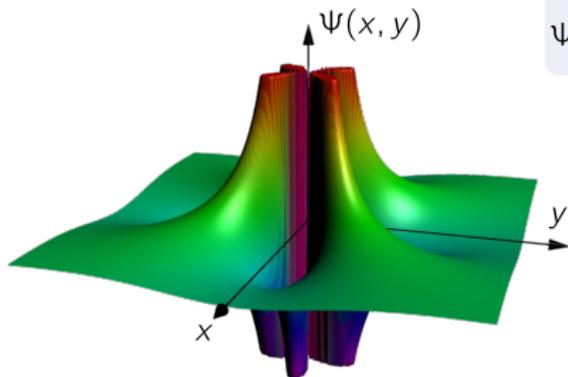
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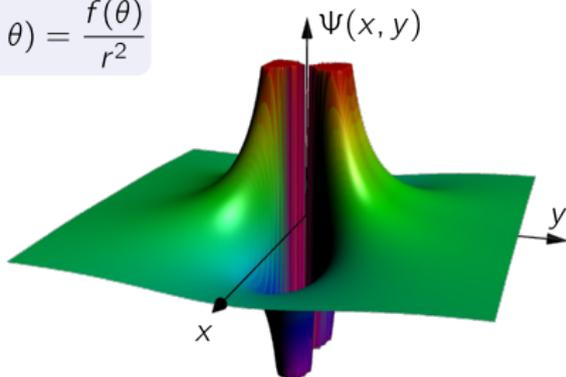
$$\boldsymbol{\epsilon} = a\boldsymbol{\sigma} + b\text{Tr}(\boldsymbol{\sigma})\mathbf{1}$$

$$\mathcal{O}(\mathbf{q}) = \frac{1}{q^2} \begin{pmatrix} q_y^2 & -q_x q_y \\ -q_x q_y & q_x^2 \end{pmatrix} = \begin{pmatrix} \sin(\omega)^2 & -\sin(\omega) \cos(\omega) \\ -\sin(\omega) \cos(\omega) & \cos(\omega)^2 \end{pmatrix}$$



shearing

$$\Psi(r, \theta) = \frac{f(\theta)}{r^2}$$



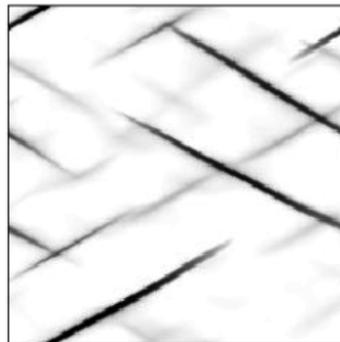
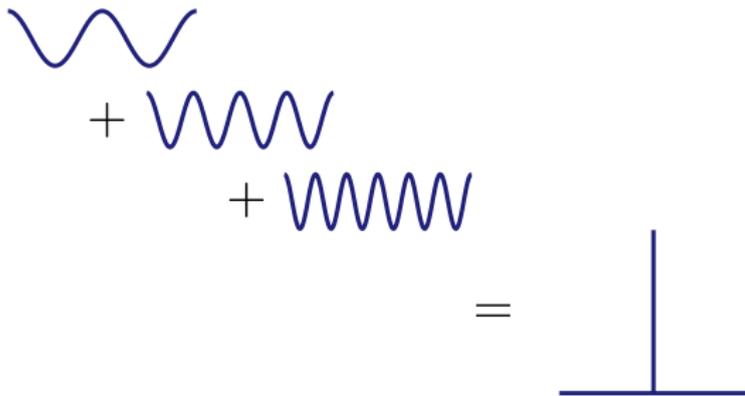
uniaxial traction

## 2d model: kernel behavior

- The kernel depends only on the angle  $\omega$  of the wavevector  $\mathbf{q}$ :

$$\tilde{\Psi}_d(\mathbf{q}, \omega) = \tilde{\psi}_d(\omega).$$

- At instability, all the wavelength with the same angle diverge: **localization** along bands.

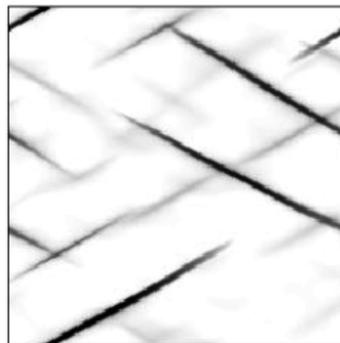
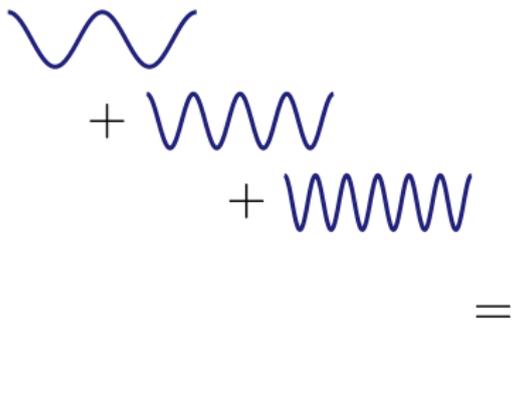


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- The **critical damage** for localization and the **orientation of the localization band** can be predicted.
  - 45° for shearing, 57° for uniaxial tension.

# Conclusion

For any damage model, the elastic kernel can be computed  
⇒ **Elastic interface** model for damage evolution.

**Localization** comes from an **elastic kernel instability**.

## Future work

How is this new kind of transition related to the observed avalanches statistics?

### Avalanches in the 1d model

