

Kinetic Theory of a Non-spherical Granular Intruder

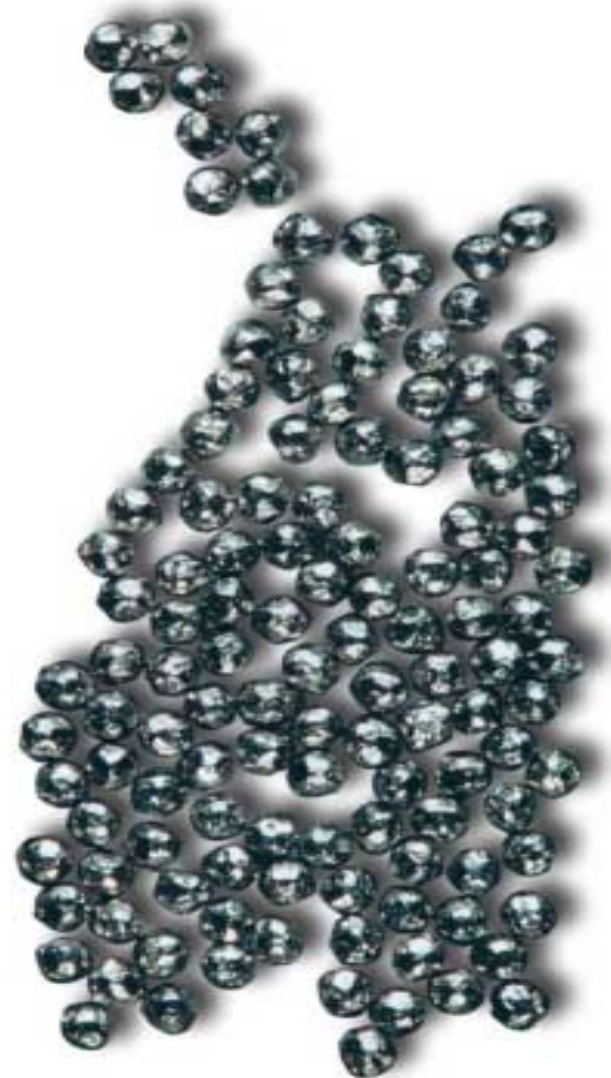
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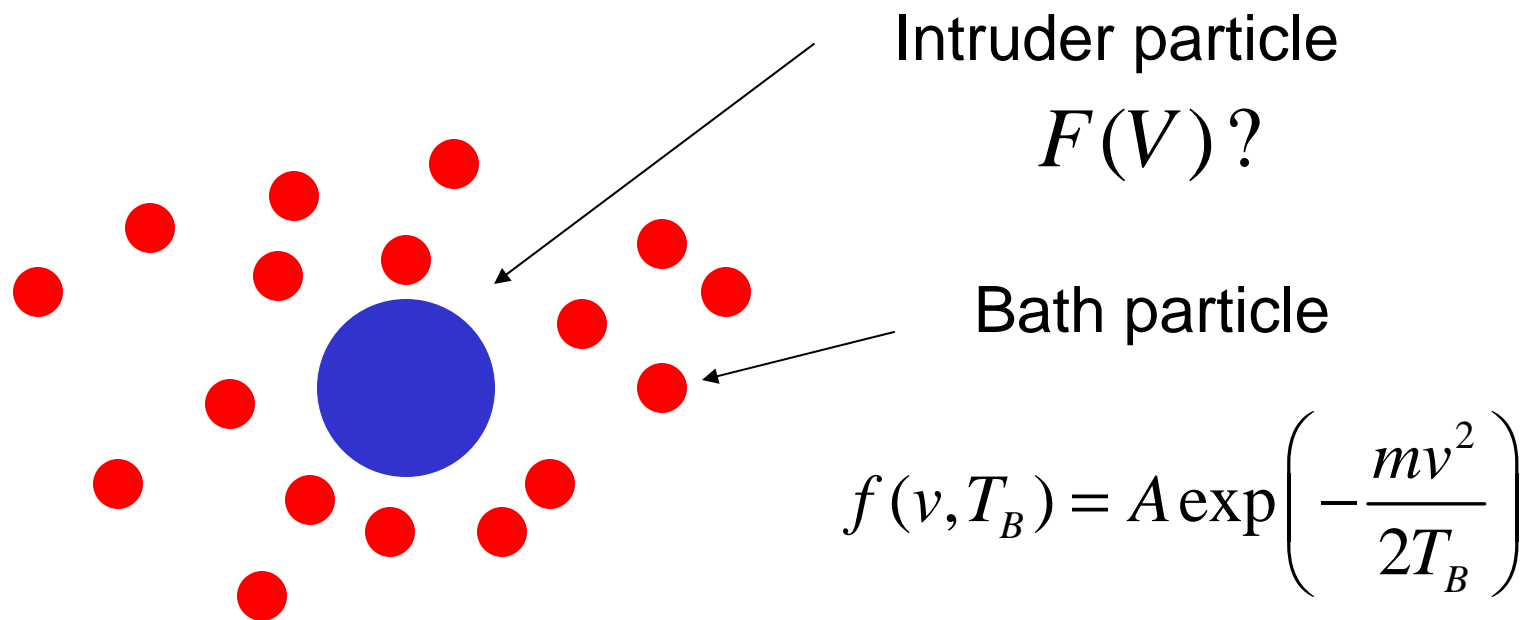
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Non-spherical Granular Systems



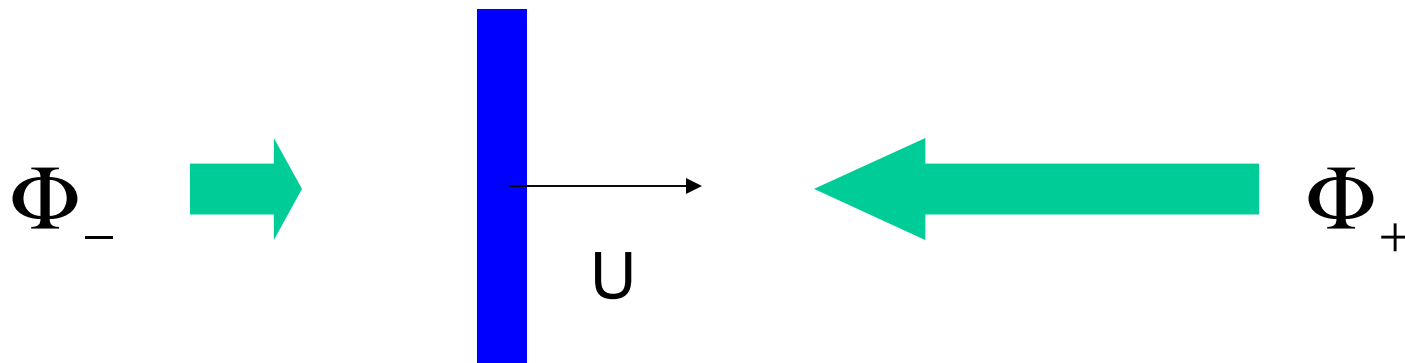
Stationary granular gas



Intruder-bath particle collisions are inelastic with COR $\alpha < 1$

Martin and Piasecki, 1999; Garzo and Dufty, 1999; Barrat and Trizac, 2002

Particle flux depends on surface velocity



$$\Phi(U) = \Phi_+ + \Phi_- = \sqrt{\frac{m}{2\pi T}} \exp\left(-\frac{mU^2}{2T}\right) + U \operatorname{erf}\left(U \sqrt{\frac{m}{2T}}\right)$$

$$P_+(U) = \frac{\Phi_+}{\Phi} = \frac{1}{2} \left(1 + \frac{U}{\Phi(U)} \right)$$

Kinetic Equation

$$\frac{\partial F(U, t)}{\partial t} = -\Phi(U)F(U, t) + \int_{-\infty}^{\infty} \Psi(V \rightarrow U)F(V, t)dV$$

↑
↑
Intruder particle velocity distribution
Transition rate

$$\Psi_+(V \rightarrow U) = \rho \int_{-\infty}^V dv (V - v) f(v, a) \delta(V - U + \frac{1 + \alpha}{1 + M} (v - V))$$

$$-\Phi(U)F(U) + \rho \left(\frac{1 + M}{1 + \alpha} \right)^2 \int_{-\infty}^{\infty} dV |U - V| f(V + \frac{1 + M}{1 + \alpha} (U - V), a) F(V) = 0$$

Solution

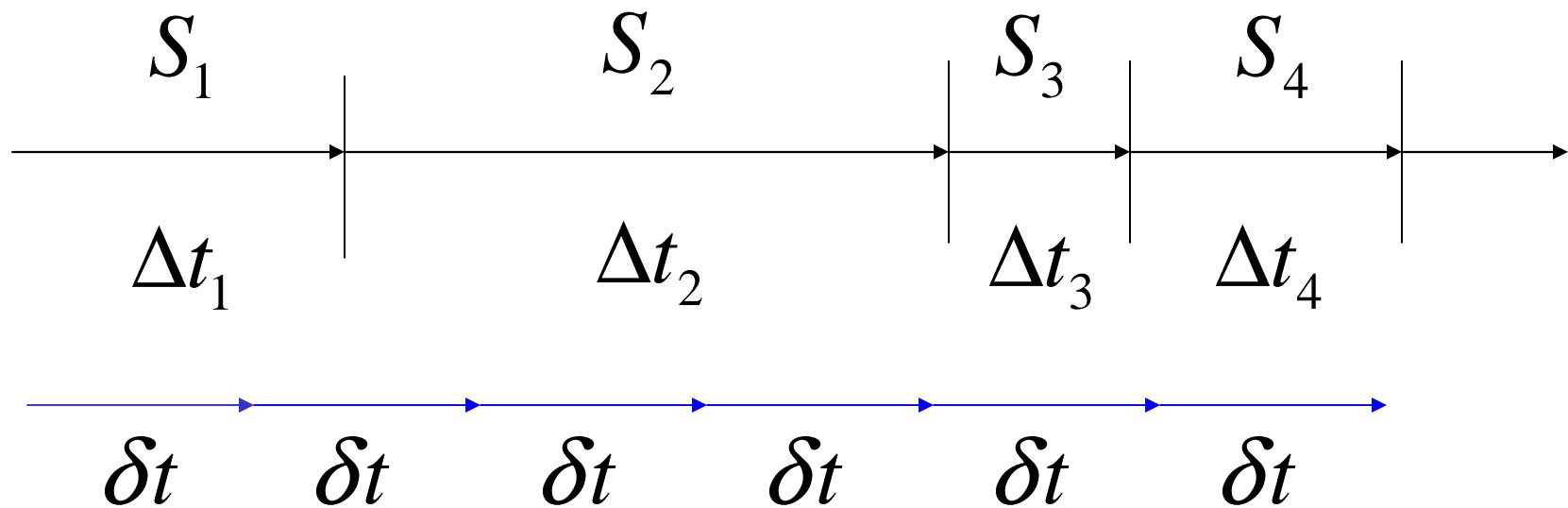
$$F(U) = \exp\left(-\frac{mU^2}{2\gamma T_B}\right)$$

The intruder particle possesses a stationary Maxwellian velocity distribution with an effective granular temperature $T_{\text{eff}} = \gamma T_B$

$$\gamma = \frac{1 + \alpha}{2 + (1 - \alpha)\frac{m}{M}} \leq 1$$

Martin and Piasecki

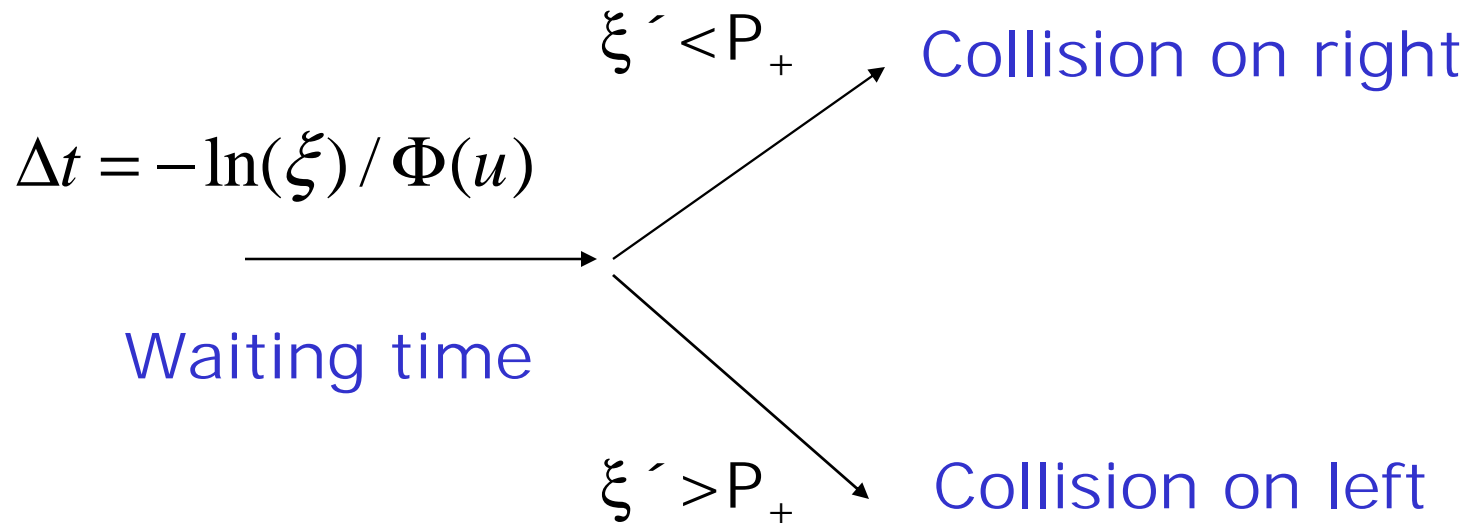
Event driven simulation

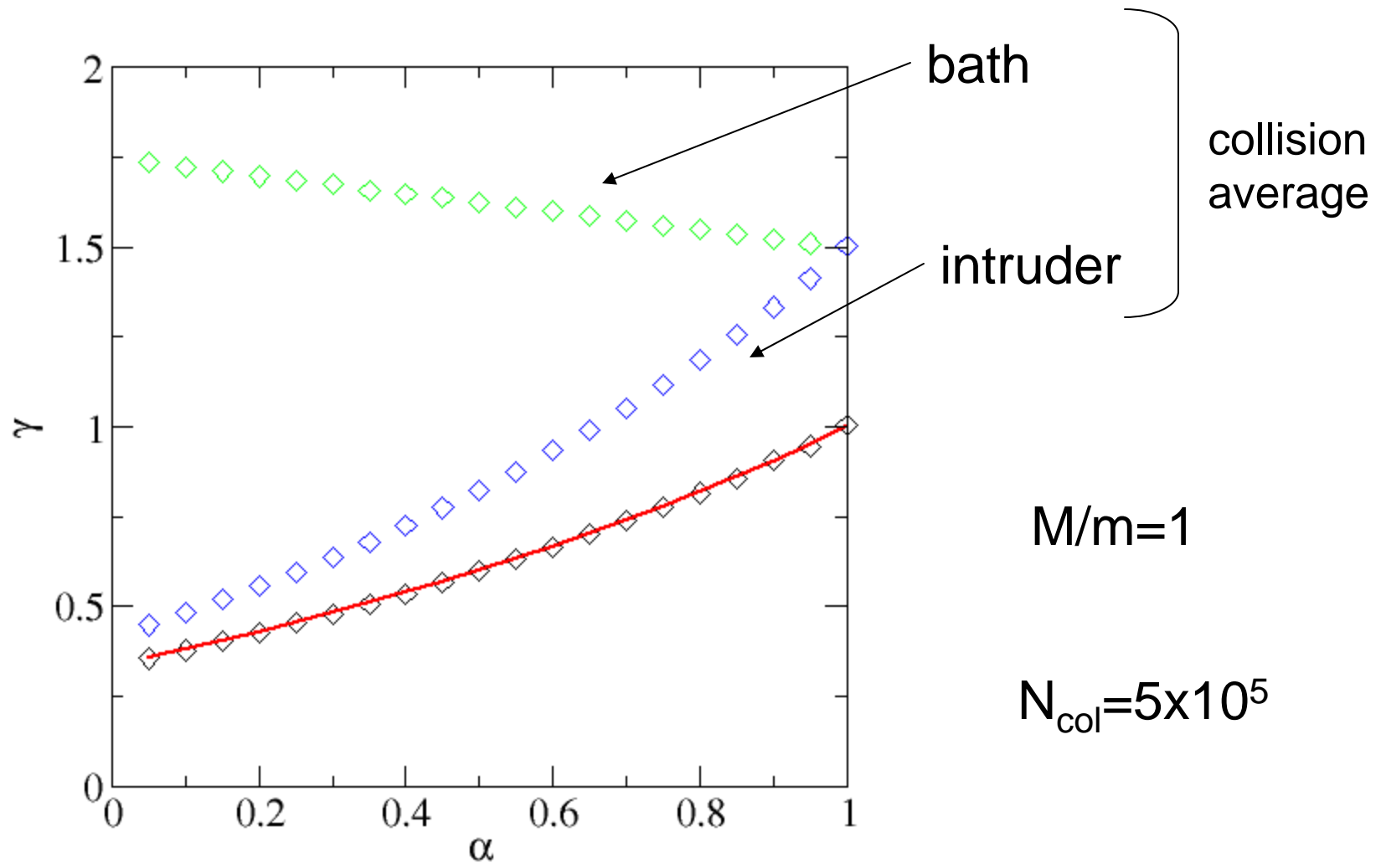


$$P(\Delta t) = \exp(-R(S_i)\Delta t)$$

Mean event rate

ED simulation



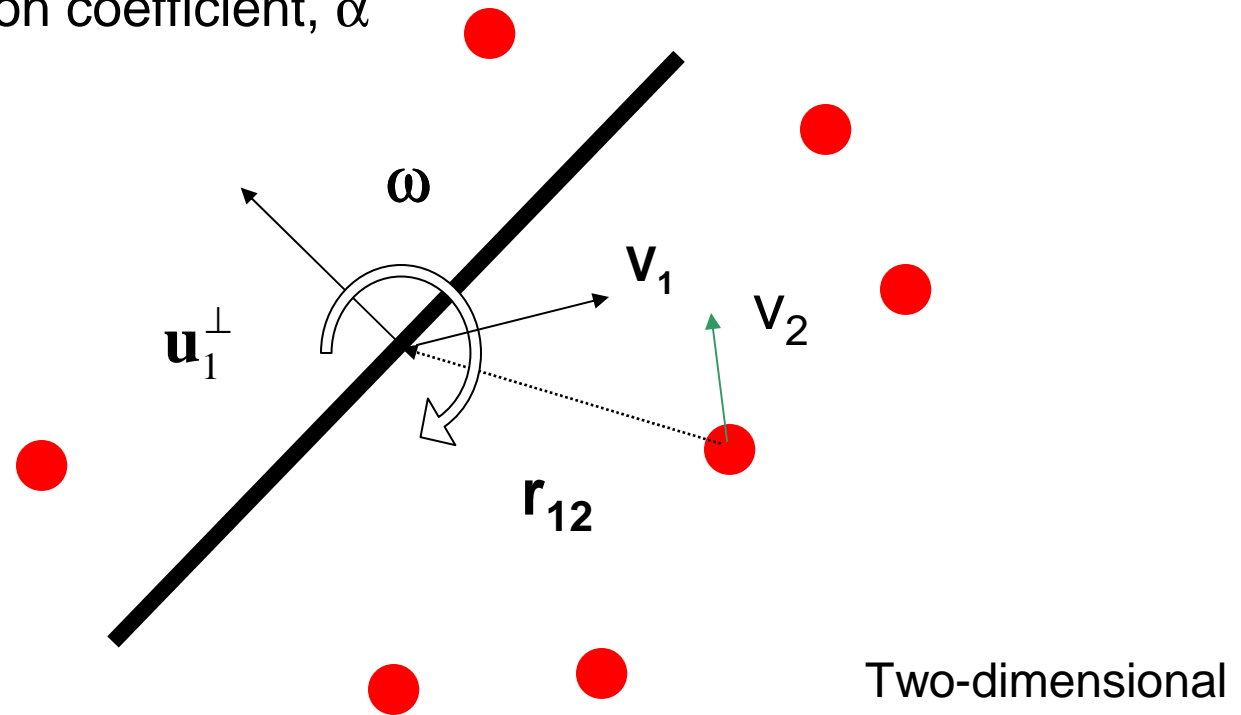


Needle System

Needle length, L

Moment of inertia, I

Normal restitution coefficient, α

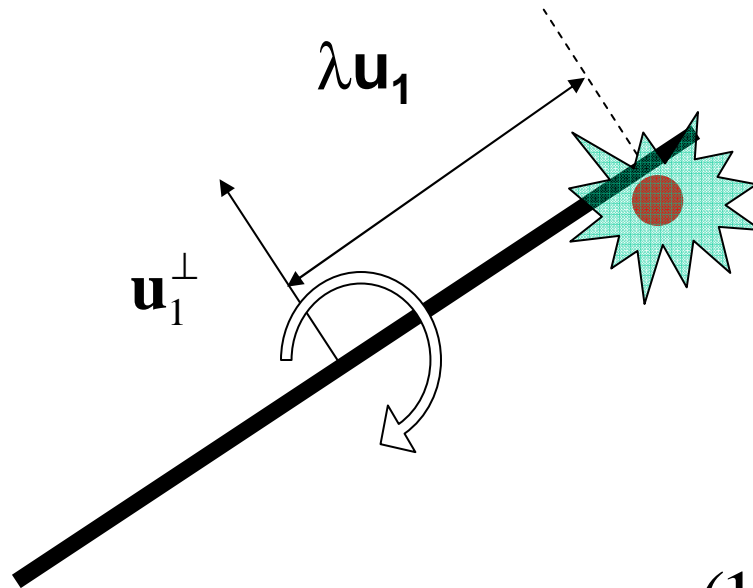


Collision

$$\mathbf{V} = \mathbf{v}_{12} + \lambda \dot{\mathbf{u}}_1$$

$$\mathbf{V}' \cdot \mathbf{u}_1^\perp = -\alpha \mathbf{V} \cdot \mathbf{u}_1^\perp$$

$$\mathbf{V}' \cdot \mathbf{u}_1 = \mathbf{V} \cdot \mathbf{u}_1$$



$$\Delta p = -\frac{(1 + \alpha) \mathbf{V} \cdot \mathbf{u}_1^\perp}{\frac{1}{M} + \frac{1}{m} + \frac{\lambda^2}{I}}$$

Kinetic Theory

$$\frac{\partial f^{(1)}(v_1, \omega)}{\partial t} = \int dv_2 \int dr_2 \overline{T_{12}} f^{(2)}(v_1, \omega, v_2)$$

$$f^{(2)}(v_1, \omega, v_2) = f^{(1)}(v_1, \omega) \Phi(v_2)$$

$$\Phi(v_2) \propto \exp\left(-\frac{mv_2^2}{2T}\right)$$

Analysis

$$\frac{dT_T}{dt} \propto \int dr_2 \int dv_2 \int d\omega \int d\theta \overline{T_{12}} f^{(2)}(v_1, \omega, v_2) E_1^T = 0$$
$$\frac{dT_R}{dt} \propto \int dr_2 \int dv_2 \int d\omega \int d\theta \overline{T_{12}} f^{(2)}(v_1, \omega, v_2) E_1^R = 0$$

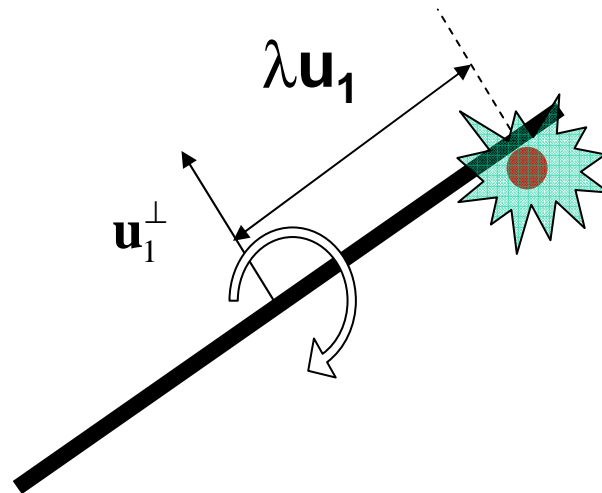
Maxwell distribution of needle angular and translational velocities is not a stationary state of the Enskog-Boltzmann Equation

But we use it as a trial function...

$$f^{(1)}(v_1, \omega_1) \propto \exp\left(-\frac{Mv_1^2}{2\gamma_T T} - \frac{I\omega_1^2}{2\gamma_R T}\right)$$

Collision Operator

$$T_{12} = \underbrace{\Theta(L/2 - |\lambda|)}_{\text{contact}} \underbrace{\delta(|\mathbf{r}_{12} \cdot \mathbf{u}_1^\perp| - 0^+)}_{\text{flux}} \underbrace{\left| \frac{d|\mathbf{r}_{12} \cdot \mathbf{u}_1^\perp|}{dt} \right|}_{\text{approach}} \underbrace{\Theta\left(-\left| \frac{d|\mathbf{r}_{12} \cdot \mathbf{u}_1^\perp|}{dt} \right|\right)}_{\text{difference}} (b_{12} - 1)$$



Solution

$$\text{Let } k = \frac{L^2}{4I(1/m + 1/M)}$$

$$b \int_0^1 dx \frac{\sqrt{1 + akx^2}}{1 + kx^2} = \frac{1 + \alpha}{2} \int_0^1 dx \frac{(1 + akx^2)^{3/2}}{(1 + kx^2)^2} \quad (1)$$

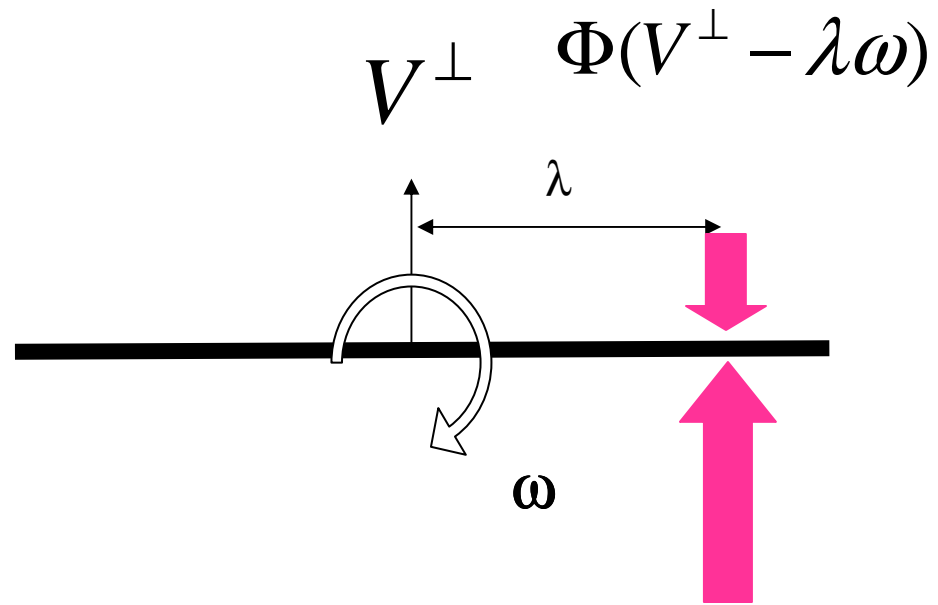
$$a \int_0^1 dx x^2 \frac{\sqrt{1 + akx^2}}{1 + kx^2} = \frac{1 + \alpha}{2} \int_0^1 dx \frac{x^2 (1 + akx^2)^{3/2}}{(1 + kx^2)^2} \quad (2)$$

$$a = \gamma_R \frac{M + m}{M + m\gamma_T} \quad (3)$$

$$b = \gamma_T \frac{M + m}{M + m\gamma_T} \quad (4)$$

Solve (2) for a . Then find b from (1). Then find γ_R and γ_T from (3) and (4)

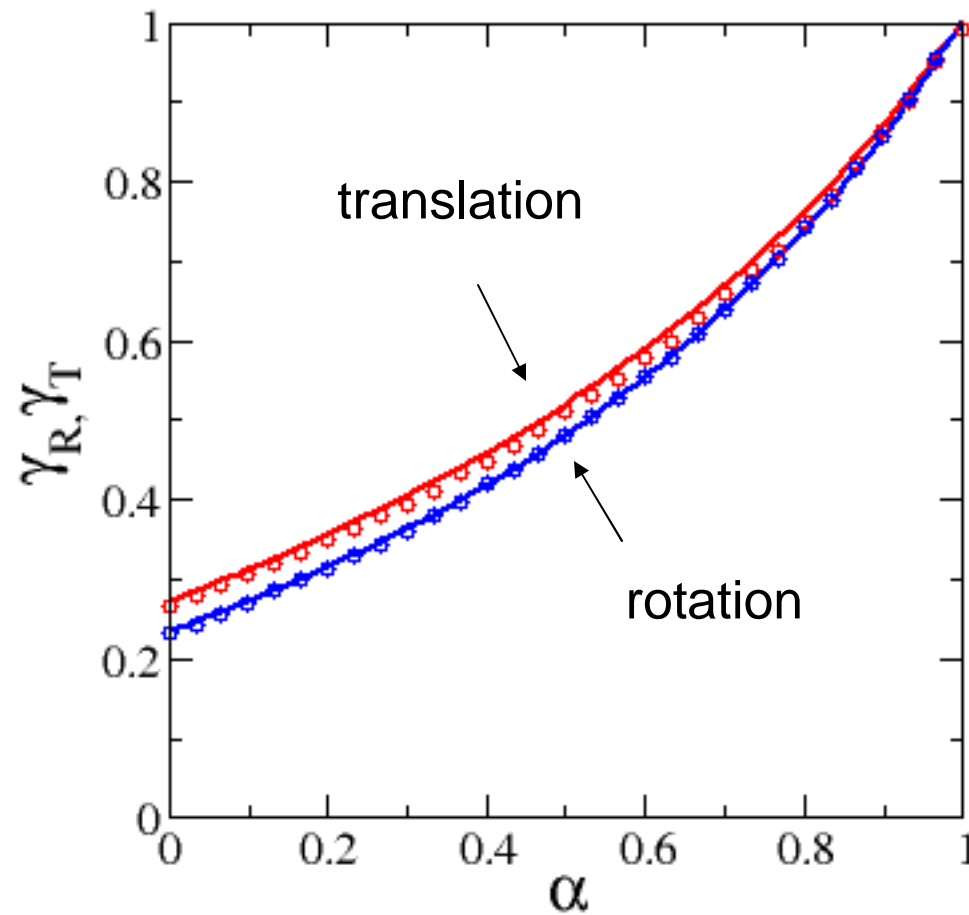
ED Simulation



Complication: flux is not constant

$$P(t) = \exp\left(-\int_0^t \Phi(t') dt'\right)$$

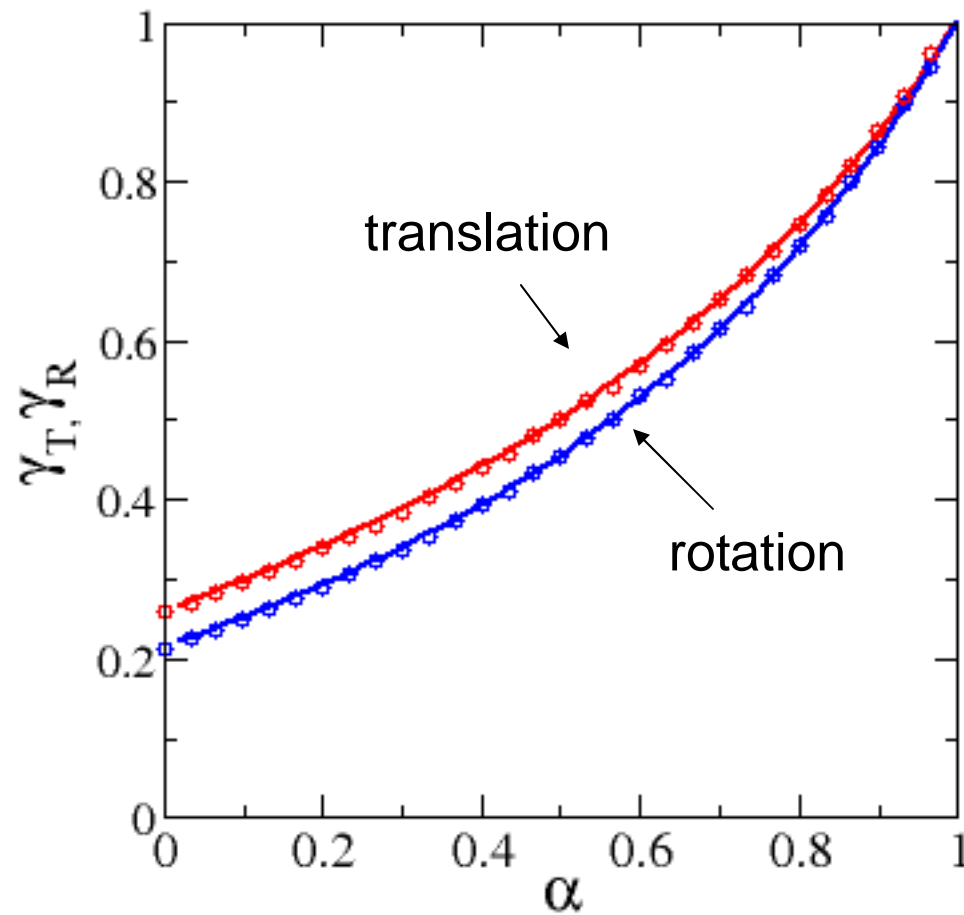
Granular temperatures



$$M=m$$

$$I = \frac{Ml^2}{12}$$

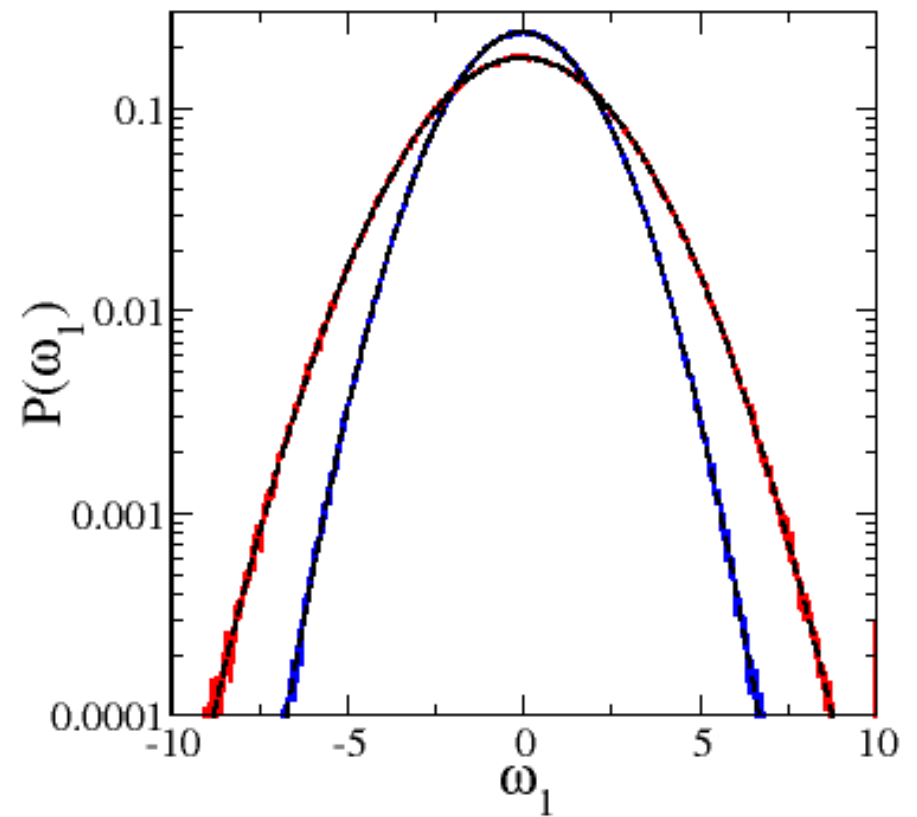
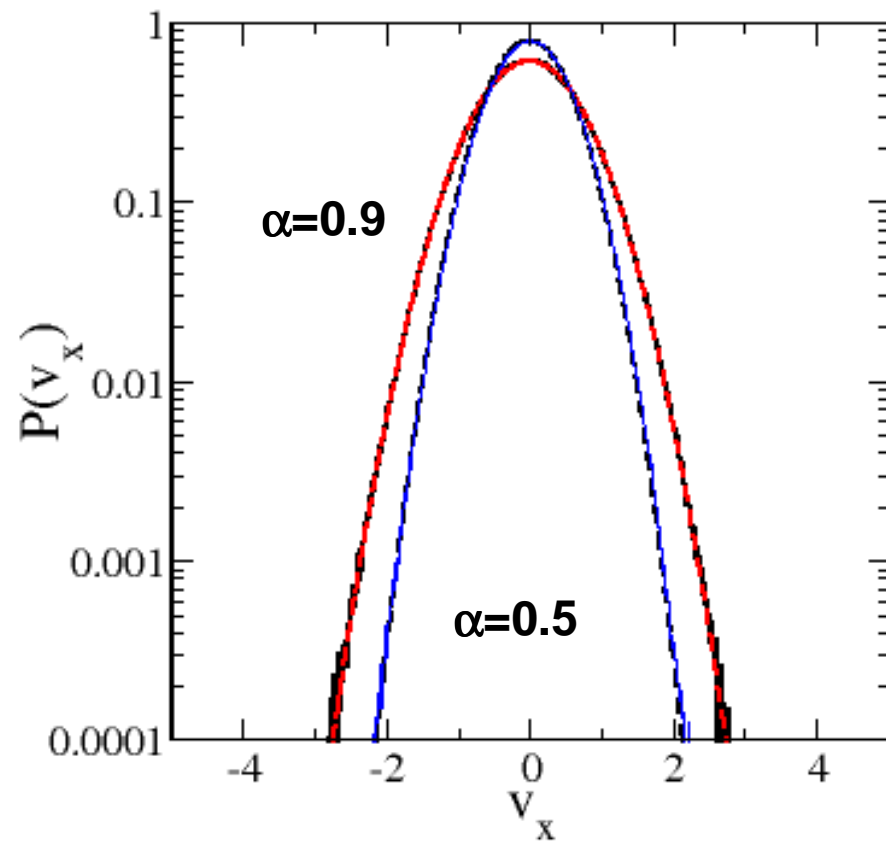
Inhomogeneous Needle



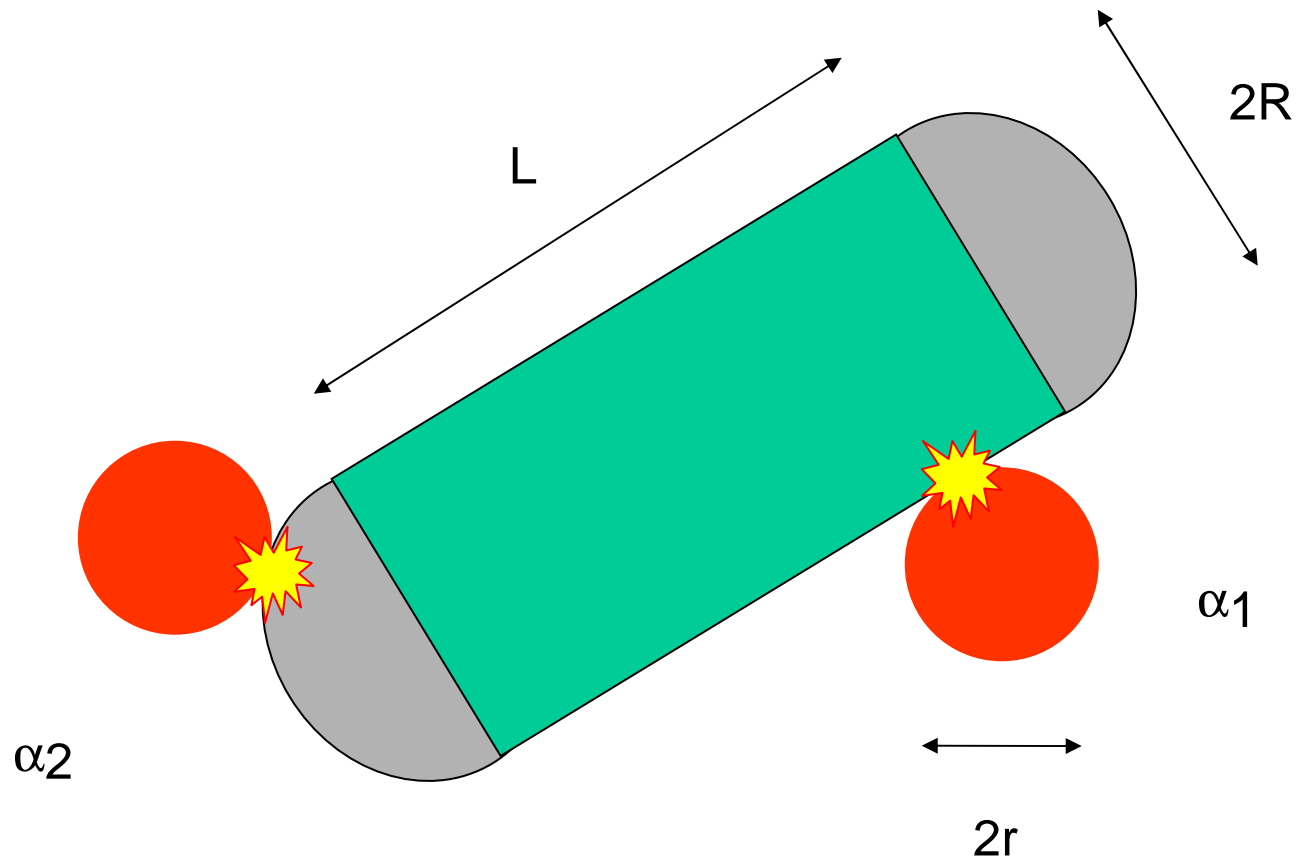
$$M = m$$

$$I = \frac{Ml^2}{16}$$

Velocity distributions



Discorectangle

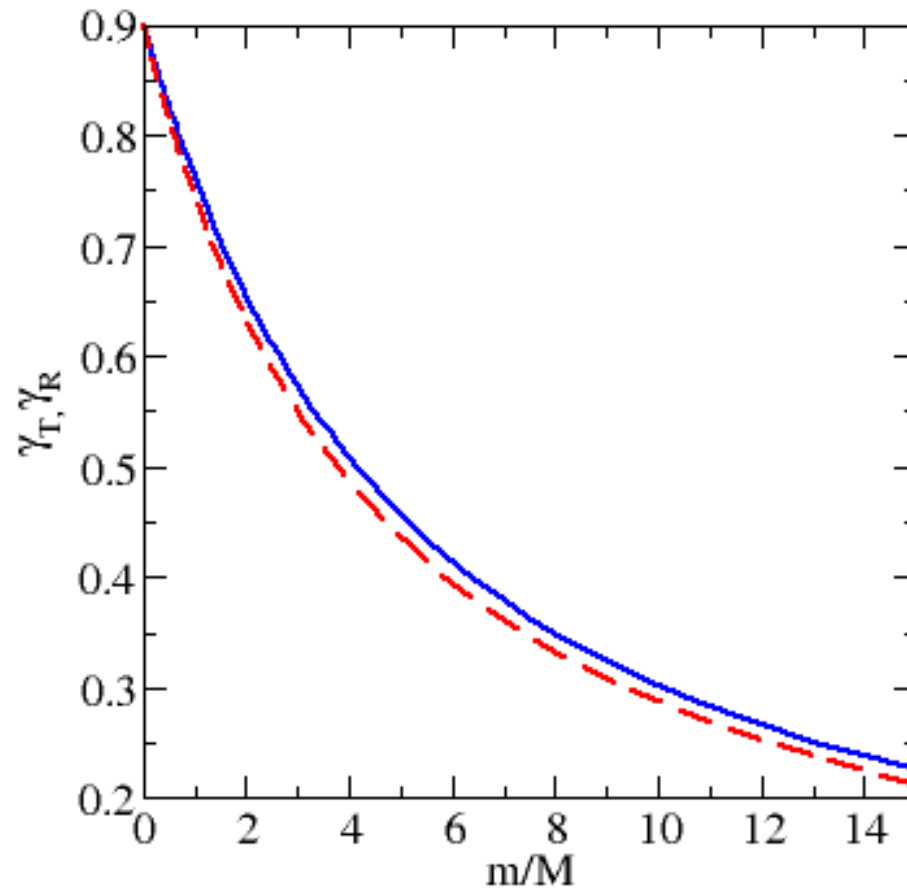


Steady State Solution

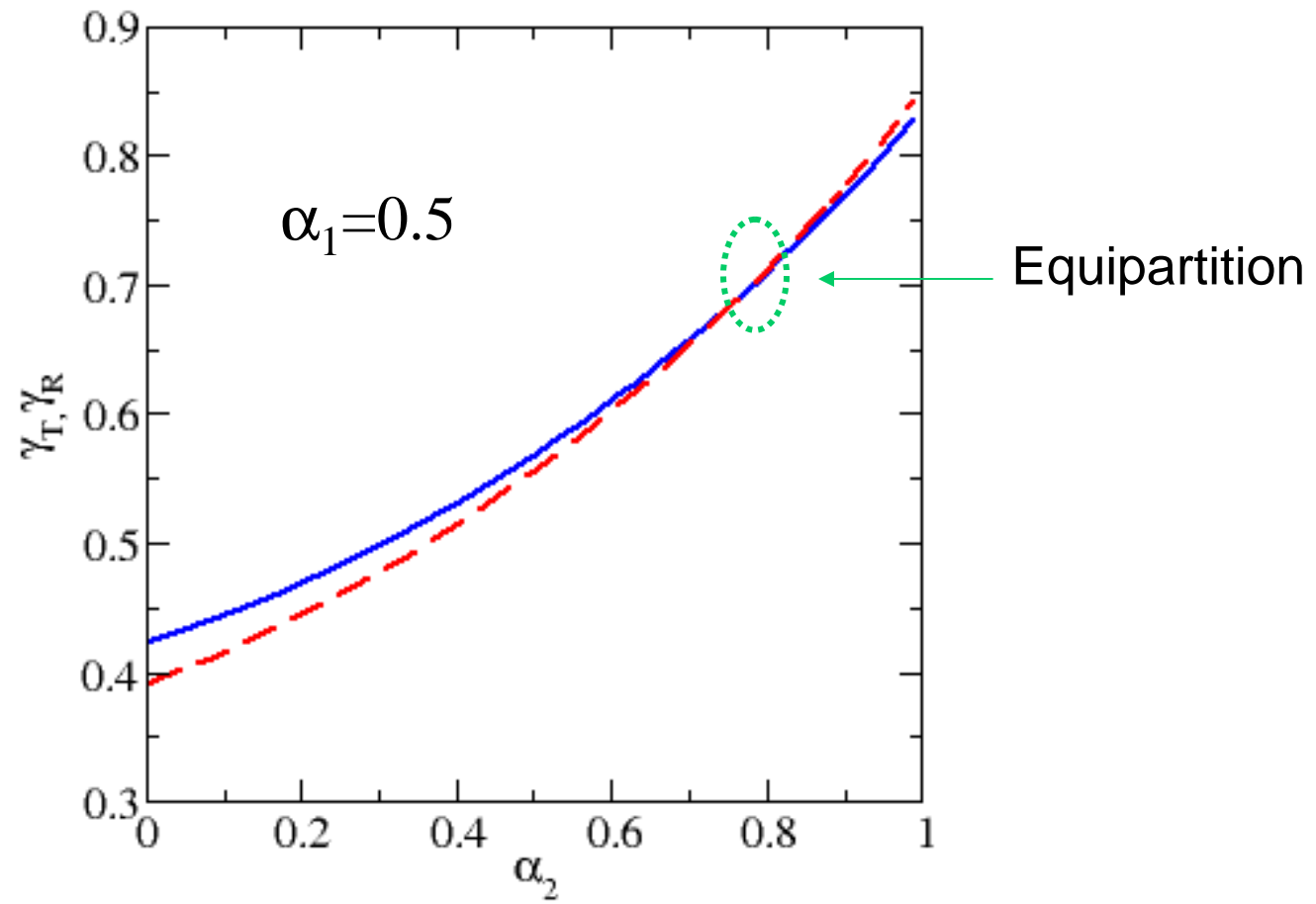
$$b[(1 + \alpha_1)cI_1^{01}(a, k) + (1 + \alpha_2)(1 - c)J_1^{01}(a, k)] = \frac{(1 + \alpha_1)^2}{2}cI_2^{03}(a, k) + \frac{(1 + \alpha_2)^2}{2}(1 - c)J_2^{03}(a, k)$$
$$a[(1 + \alpha_1)cI_1^{11}(a, k) + (1 + \alpha_2)(1 - c)J_1^{11}(a, k)] = \frac{(1 + \alpha_1)^2}{2}cI_2^{13}(a, k) + \frac{(1 + \alpha_2)^2}{2}(1 - c)J_2^{13}(a, k)$$

$$k = \frac{L^2}{4I \left(\frac{1}{m} + \frac{1}{M} \right)} \quad c = \frac{L}{L + 2(r + R)}$$

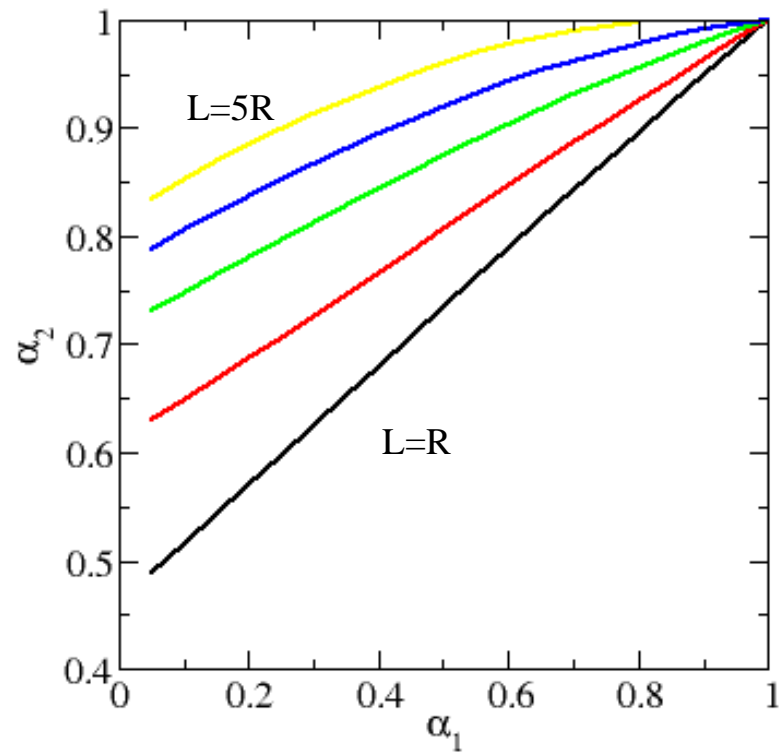
$$\alpha_1 = \alpha_2; c=4/7$$



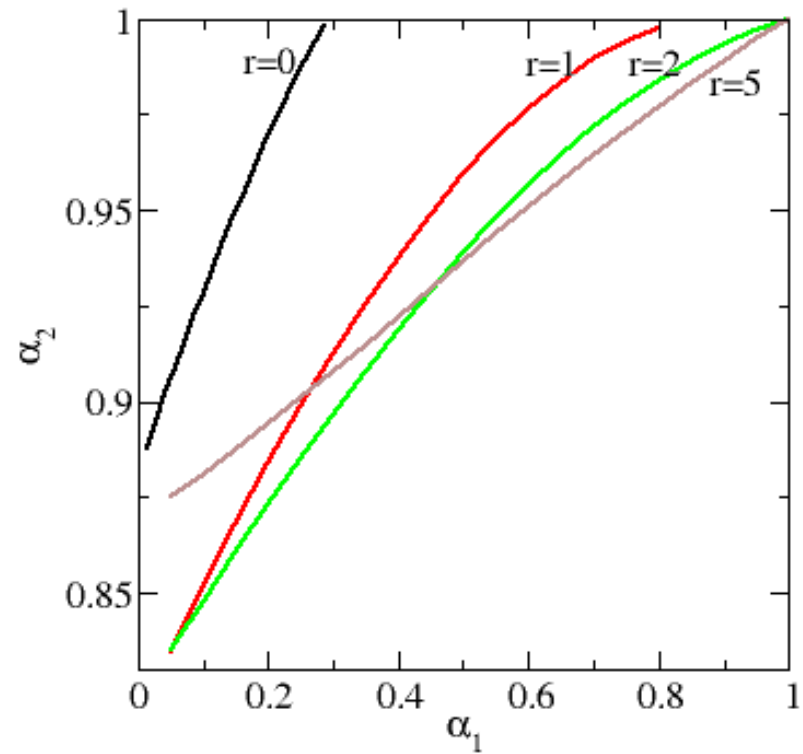
$$M = m, L = 2R, R = r$$



$m = M, r = R$



$m = M, L = 8R$



Summary

- Theory gives results in excellent agreement with ED simulations
- Equipartition is generally not obtained except:
 - in the limit of light bath particles
 - If COR depends on position of impact
- For uniform COR, $T_R < T_T$
- Small deviations from gaussian
- Non equipartition also expected for higher dimensions and more complex shapes
- Experimental verification in 2D?