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Hey, it's a workshop, so let's go off topic

Brief Interlude on Dissipation



The principal result of reviewing the experimental data is that for many solids...the specific dissipation function is independent of frequency– a generalization well known to engineers but largely neglected in physical theories of attenuation, Knopoff and MacDonald, 1958

Two Possible Scenarios for Dissipation



Broad spectrum of dampers

(Jackle, 1972)

$$\alpha = g\pi\omega/4c$$

$$v = 1 - (g/2) \ln[(\omega^2 + b_{max}^2)/(\omega^2 + b_{min}^2)]$$

And now back to what I was asked to speak about....

Continuum Fracture Mechanics





- Initiation of fracture depends upon energy (Griffith)
- Energy and (singular) stress criteria are identical (Irwin)
- Structure of stress near crack tips is universal (Irwin and Rice)

Continuum Fracture Mechanics



- Microscopic unknowns bundled into one number toughness – that can be tabulated from tests on standard specimens.
- Crack driving forces computed through continuum mechanics and finite elements in arbitrary geometries



- Rough equations of motion (Mott 1948, Dulaney and Brace, 1960)
- Dynamic calculation of stress fields (Yoffe 1951)
- Limiting speed 60% of shear wave speed (Schardin, 1955)
- Rayleigh wave speed should be limit (Stroh, 1957)
- Exact equation of motion: crack tip has no inertia (Kostrov, 1966 Eshelby, 1969)
- Extension of exact results to Mode I (Freund, Kostrov, 1974)



Net results:

- For semi-infinite crack in infinite plate, can compute energy flowing to tip of straight crack moving with velocity v(t) for arbitrary time-dependent loading on crack faces.
- Crack velocity and path are given.
- Assumption plate is infinite is not mere technicality.
- Energy cost function $\Gamma(v)$ closes theory.
- Many felt $\Gamma(v)$ had to be largely independent of velocity, but nothing in structure of theory demanded this



Gol'dstein and Salganik, 1974

- Crack moves along a path such that K_{II} vanishes
- Energy consumption maximized in this direction
- Seed cracks placed in mixed mode loading kink in expected direction





- Equation of motion for small deviations from straightness (Rice and Cotterell, 1980)
- Upper cutoff on curvature and extension to three dimensions (Sethna and Hodgdon, 1993)
- Generalization to dynamic fractures (Adda-Beddia, Ben-Amar, and Lund 1999; Oleaga, 2001)





- Industrial applications rely mainly on simple strength of materials analysis, or in critical applications on continuum fracture mechanics
- Continuum analysis handles complex geometries and loading better than any other framework.
- Hence beliefs widely held though rarely stated:

Real materials are not made of atoms! or In fracture atoms matter, for materials that don't!



- Static Cracks: Compute criterion for initiation (usually one number)
- Dynamic Cracks: Compute speed from driving force (usually a function of one variable)
- ... and probably for both Static and Dynamic: Compute crack path (functions of several variables)



Physics of fracture

A physically based theory of brittle fracture cannot be created entirely within a continuum description.



The cohesive forces between atoms rise and fall on the scale of atomic separations.





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Modeling should not be grid-independent; nature has established a grid at the atomic scale and fracture depends upon it.

Analytical and numerical techniques allow one to move well beyond continuum analysis.



Snapping Bonds Kelvin Dissipation Acceleration $m\ddot{\vec{u}}_i = \sum_{i} \left[\vec{f}(\vec{u}_{ji}) + \vec{g}(\dot{\vec{u}}_{ji}, \vec{u}_{ji}) \right]$ Mass $\vec{g}(\vec{u}_{ji}, \vec{u}_{ji}) = \dot{\vec{u}}_{ji} \theta(u_c - u_{ji})$ f(u)| $u \xrightarrow{u_c} u$ a

MPM, International Journal of Fracture 130 517-555 (2004)



Ideal Brittle Crystal

This model can be solved *exactly* when $u_c - a \ll a$ (Slepyan, 1980... MPM, 1995...Kessler and Levine...)

Acceleration Snapping Bonds Kelvin Dissipation

Mass

$$m\ddot{\vec{u}}_i = \sum_j \left[\vec{f}(\vec{u}_{ji}) + \vec{g}(\dot{\vec{u}}_{ji}, \vec{u}_{ji})\right]$$





MPM, International Journal of Fracture **130** 517-555 (2004)



Example: for triangular lattice in Mode III $\ddot{u}_{i}^{y} = \frac{2c^{2}}{3a^{2}} \sum_{j \in n(i)} \left(u_{ij}^{y} + \beta \dot{u}_{ij}^{y} \right) \theta(\lambda_{f} - u_{ij}).$ (1)

complete solution reads

$$\tilde{v} = v/c, \quad \tilde{\beta} = \beta c/a; z = \frac{3 - \cos(\omega/\tilde{v}) - 3\omega^2/[4(1 - i\tilde{\beta}\omega)]}{2\cos(\omega/2\tilde{v})}$$
(2)

$$y = z + \sqrt{z^2 - 1} \text{ with } abs(y) > 1, ; F(\omega) = \left\{ \frac{y^{[N-1]} - y^{-[N-1]}}{y^N - y^{-N}} - 2z \right\} \cos(\omega/2\tilde{v}) + 1$$
(3)

$$Q(\omega) = \frac{F}{F - 1 - \cos(\omega/2\tilde{v})}; \tilde{\lambda}_y = \lambda_y / \sqrt{(4\lambda_f^2 - \lambda_x^2)/3}$$
(4)

$$\tilde{\lambda}_{y} = \frac{1}{\sqrt{2N+1}} \exp\left[-\int \frac{d\omega'}{4\pi} \left\{\frac{1}{i\omega'(1+\tilde{\beta}^{2}\omega'^{2})} \left[\ln Q(\omega') - \overline{\ln Q(\omega')}\right] + \frac{\tilde{\beta}\ln|Q(\omega')|^{2}}{1+\tilde{\beta}^{2}\omega'^{2}}\right\}\right]$$



Numerical Methodology



Lower row of atoms held rigid







Wiener-Hopf techniques allow 800,000,000 atom MD... on a laptop in 30 minutes





Scaling of Steady States





Silicon is "well known" to cleave cleanly along the (111) and (110) planes, but not at all along (100)

Clean failure along (110)

Rough failure along 100



Application I: single-crystal silicon

Theory and experiment for single crystal silicon may finally agree... but it seems to take quantum mechanics!





Application II: Crack-tip instability





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Application III: Self-healing pulses





Gerde and Marder, Nature 2001



Application IV: Rupture of Rubber





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 $\operatorname{cond-mat}/0504613$





















Is principle of local symmetry always correct?

In a material that is isotropic and homogeneous at the macroscopic level, do cracks always travel in the direction it predicts?

Answer: no. For example, cracks can follow crystal planes that are completely invisible to continuum elasticity

Displace upper boundary by (δ_x, δ_y)



Hold lower boundary rigid

In each case, compute shear stress versus angle, find where K_{II} vanishes

Displace upper boundary by (δ_x, δ_y)



Hold lower boundary rigid

By varying Kelvin dissipation, for fixed loading conditions, one can obtain different steady velocity solutions.

Displace upper boundary by (δ_x, δ_y)



Hold lower boundary rigid

Take height N = 200, $u_c = 1.2$, displace top by $\delta_y = 20$, and $\delta_x = .23\delta_y$. Set Kelvin dissipation to $\beta = 2$ and then to $\beta = .02$.

Displace upper boundary by (δ_x, δ_y)



Hold lower boundary rigid

Obtain cracks moving at $v/c_R = .01$ and $v/c_R = .83$.

Displace upper boundary by (δ_x, δ_y)



Hold lower boundary rigid

In each case, compute shear stress versus angle, find where K_{II} vanishes

Crack with $v = .01c_R$, should kink at -16°







However, both cracks travel straight along horizontal axis forever







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Experiments and computations in crystals clearly show macroscopic consequences of microscopic arrangement





- Range of cohesive forces and atomic spacings are the same...this causes trouble for continuum theories of brittle crack tips.
- Experiments and computations in crystals clearly show macroscopic consequences of microscopic arrangement
- Elimination of crack singularities by discreteness continues to be important even in polymeric materials, where separating units are much larger than atoms.





Atomic-scale studies answer questions about crack initiation, speed, and direction to complement continuum studies involving complex geometries and loading.

