

# Analysis of Viral Capsid Deformation



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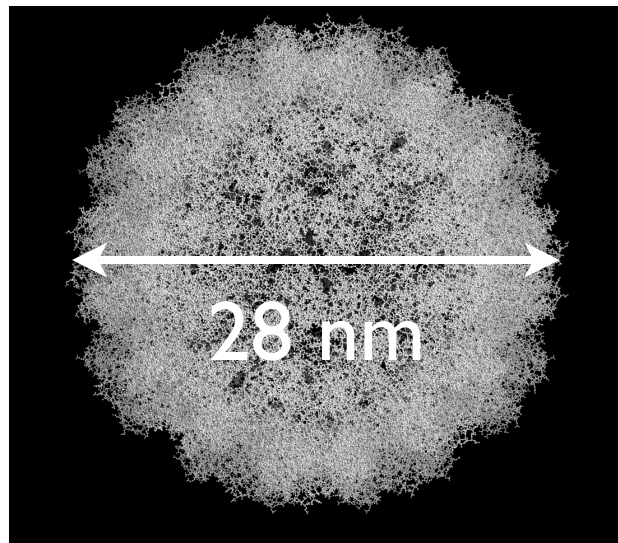
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**UCLA**

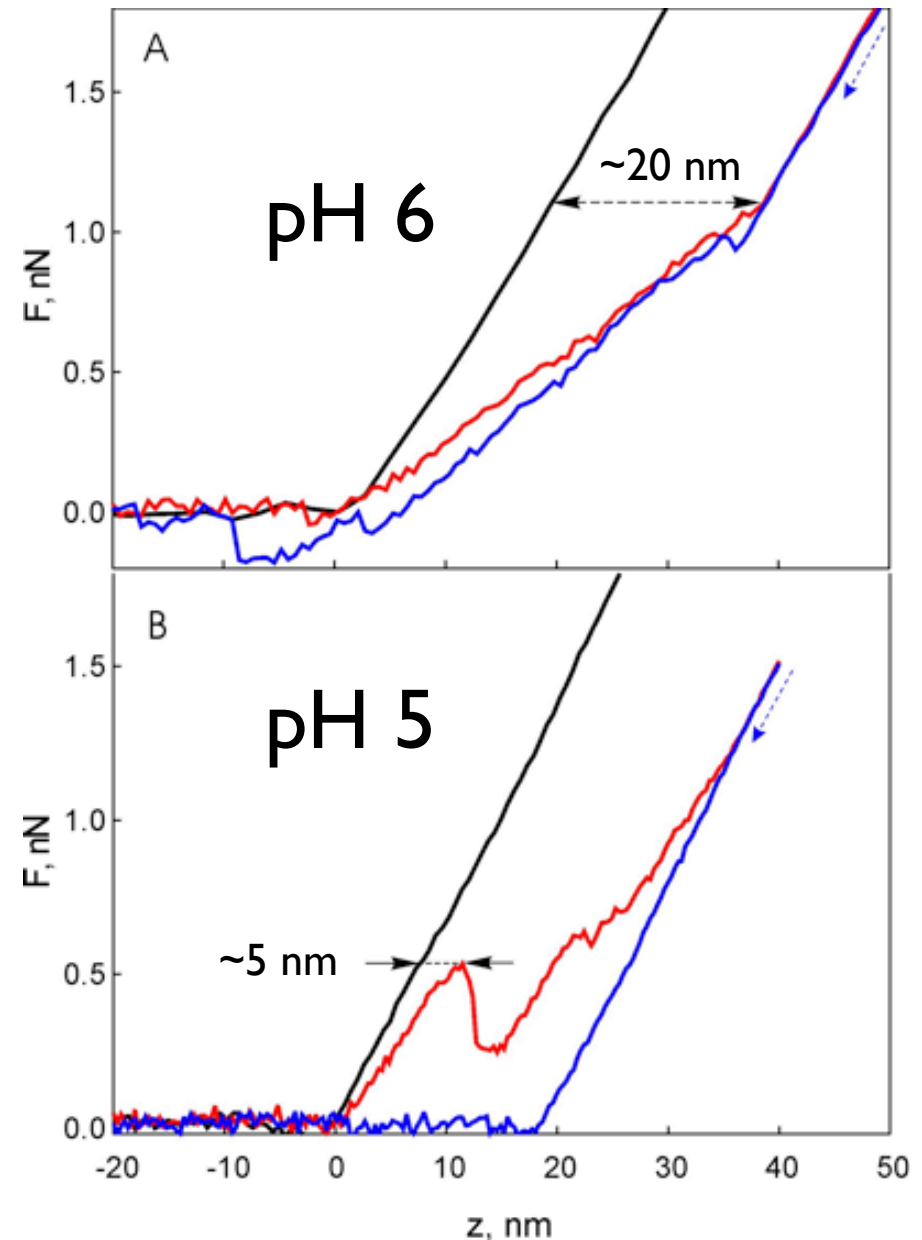


# AFM mechanical testing of CCMV

(C. Knobler, et al.)



- Linearly elastic (even for large deformation)
- Slope changes with pH
- Irreversible damage at lower pH



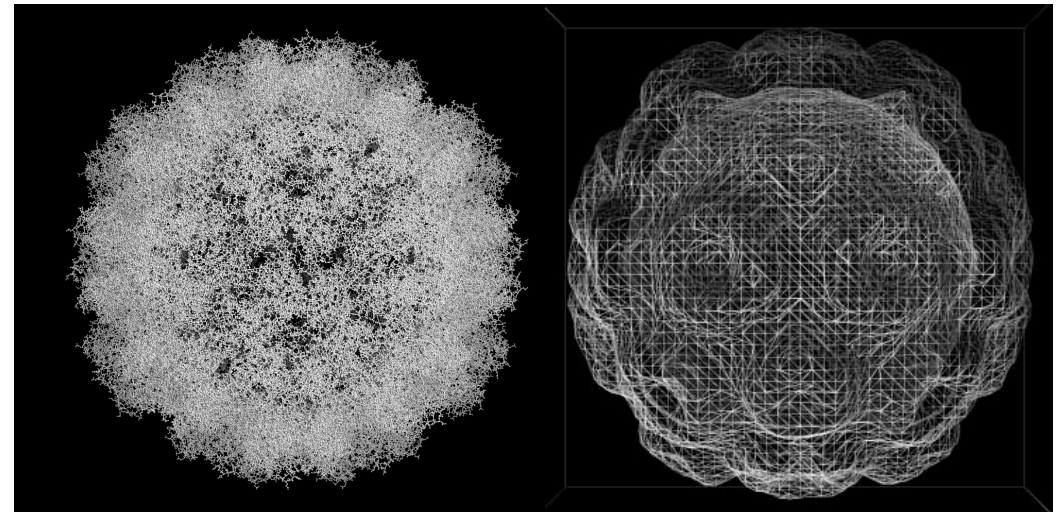
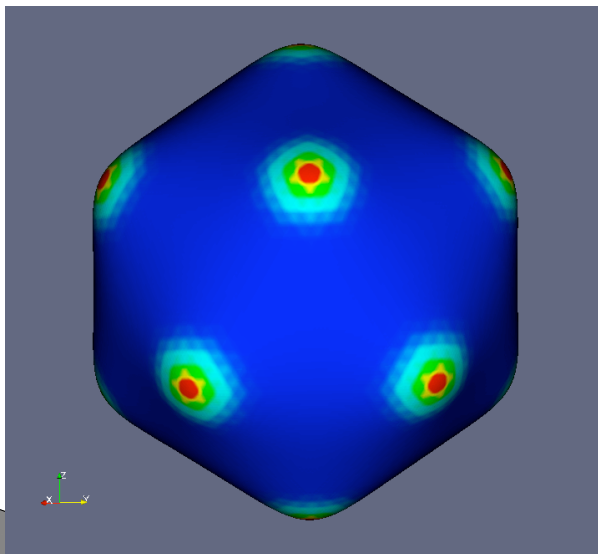
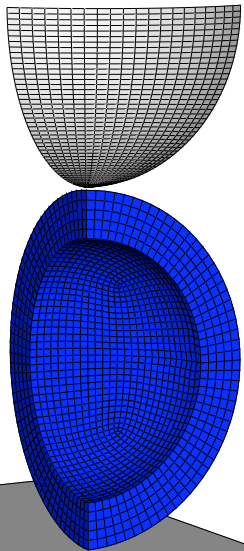
# Questions:

- Why is force response linear?
- What is responsible for damage?
- Why does damage occur only at lower pH?
- Hypothesis: (nonlinear) elasticity has something to do with this.

# The Strategy: coarse-grain

Throw away as many DOF as possible while retaining a model which has the right Physics (and Biology?).

- Continuum elasticity in 3-D and 2-D
- Multi-scale simulation



# 3-D Continuum Model: Thick Spherical Shell

After all, aren't capsids more spherical than horses?

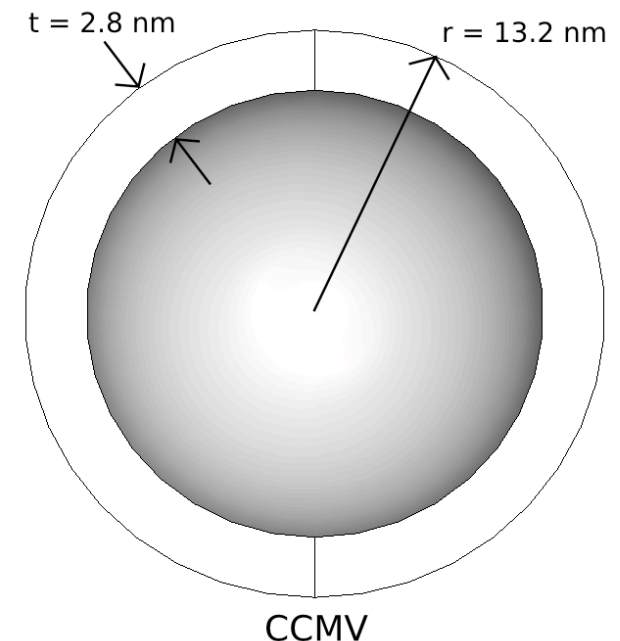
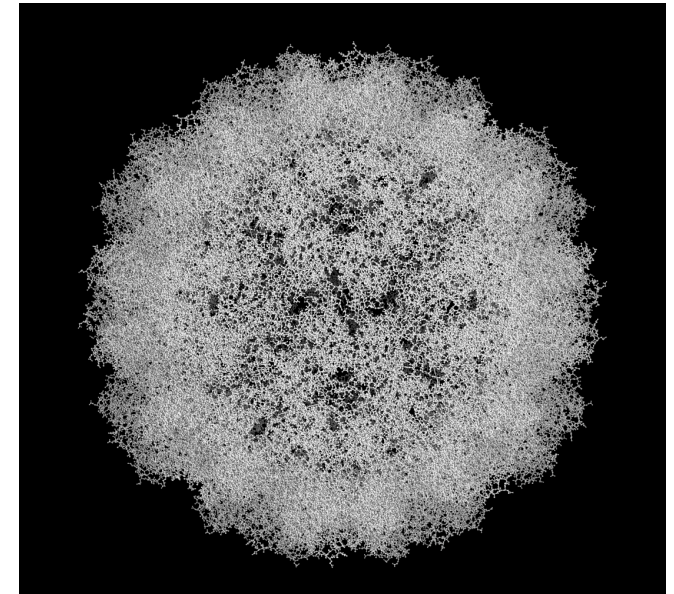
$$\mathcal{H} = \int_V w(E_{ij}) dV - W^{\text{ext}}$$

$$\mathbf{E} = \frac{1}{2} (\nabla \vec{u} + \nabla \vec{u}^T + \nabla \vec{u}^T \nabla \vec{u})$$

$\vec{u}$  = displacement field

$W^{\text{ext}}$  = work of external forces

$$\boldsymbol{\sigma} = \frac{\partial w}{\partial \mathbf{E}} = \text{stress tensor}$$





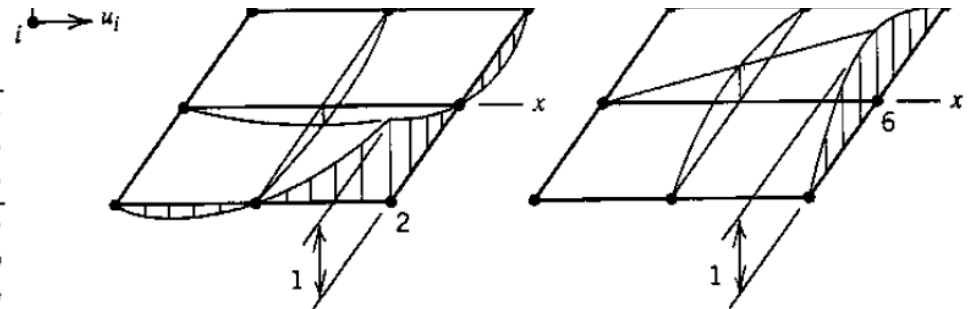
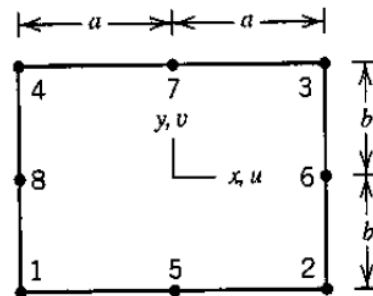
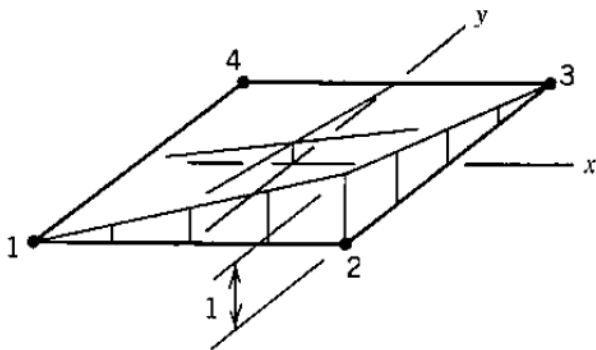
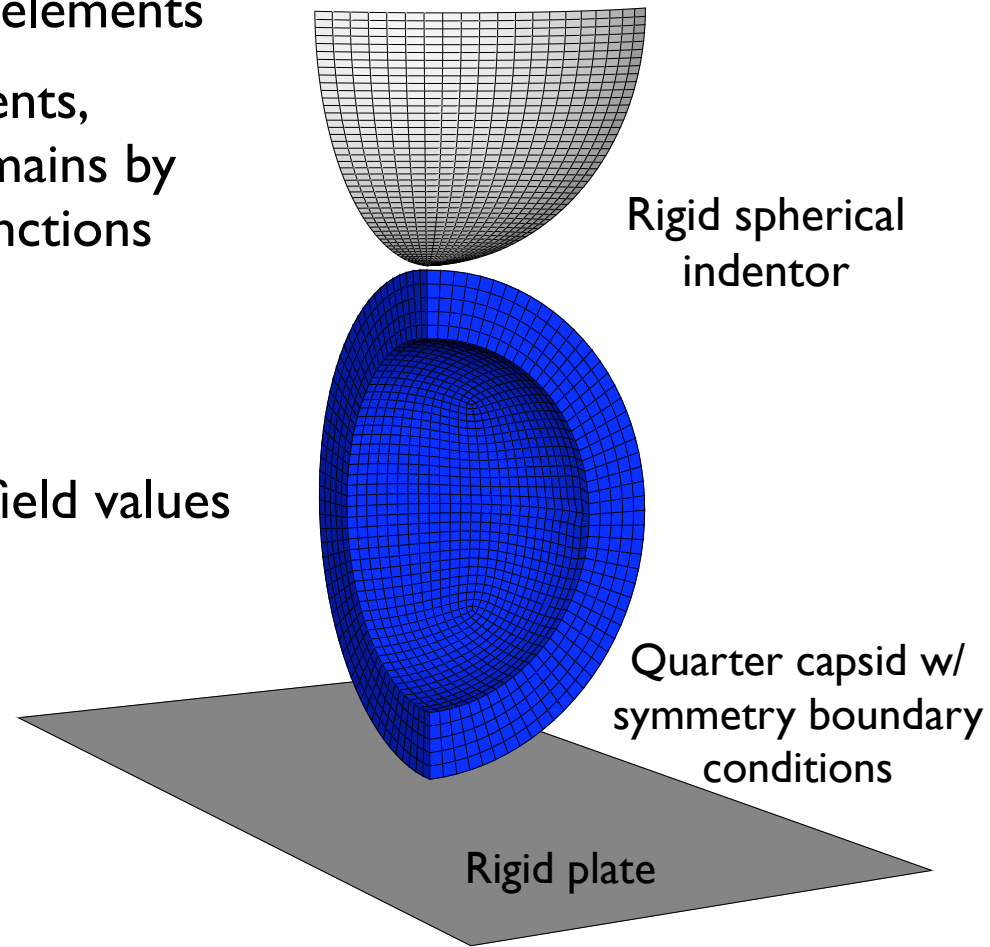
# The Finite Element Method (FEM)

- Discretize shape into simple polyhedral elements
- Approximate unknown field (displacements, deformed shape) locally on element domains by interpolation simple polynomial basis functions

$$\vec{u}(\vec{r}) = \sum_{a=1}^N \vec{u}_a N_a(\vec{r})$$

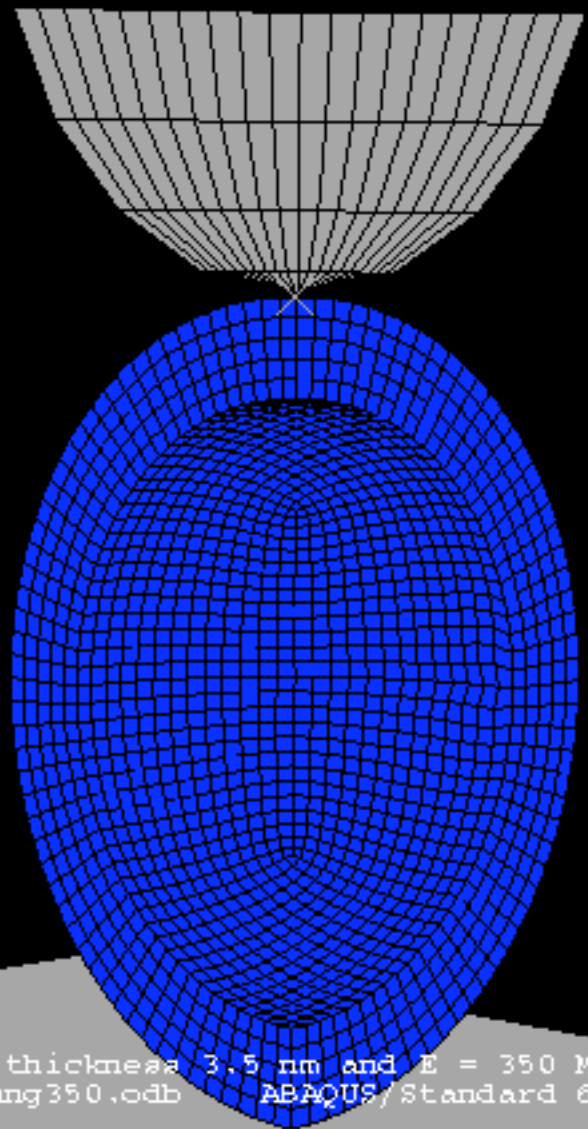
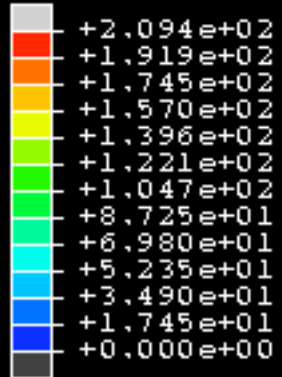
- Minimize energy with respect to nodal field values (Ritz Method)

$$\min_{\{\vec{u}_a\} \in \mathbb{R}^{3N}} \mathcal{H}$$





S, Mises  
(Ave. Crit.: 75%)

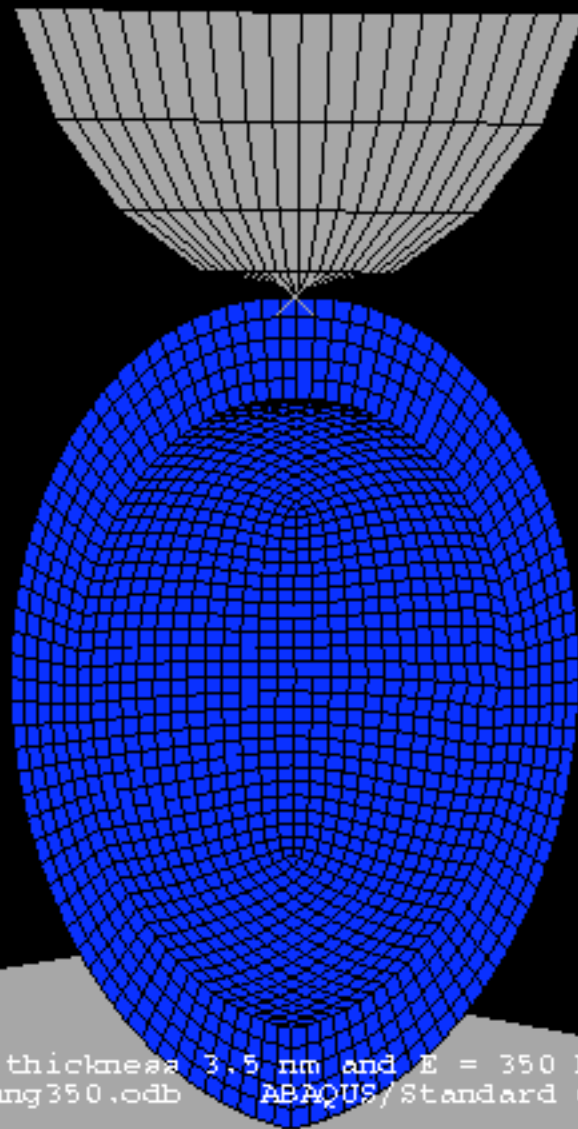
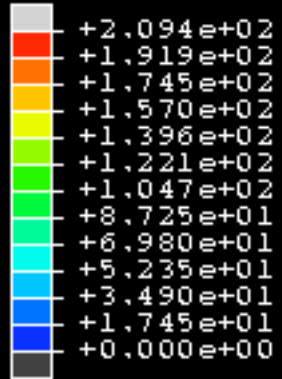


Job on capsid with thickness 3.5 nm and E = 350 MPa  
ODB: Thickness35Young350.odb ABAQUS/Standard 6.4-2 Thu Mar 10 12:45:01 PST 2005

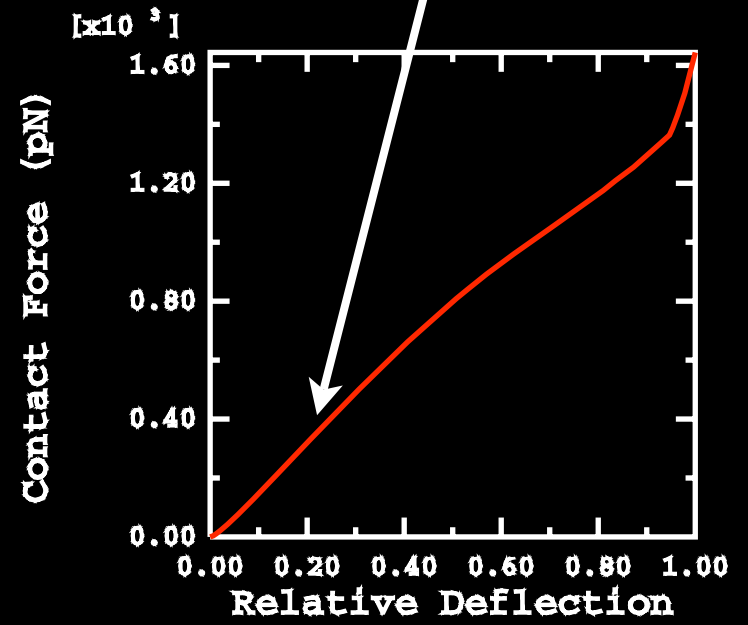
Step: Loading  
Increment 0: Step Time = 0.000  
Primary Var: S, Mises  
Deformed Var: U Deformation Scale Factor: +1.000e+00



S, Mises  
(Ave. Crit.: 75%)



**linear** for small deflections



Job on capsid with thickness 3.5 nm and E = 350 MPa  
ODB: Thickness35Young350.odb ABAQUS/Standard 6.4-2

Thu Mar 10 12:45:01 PST 2005

Step: Loading  
Increment 0: Step Time = 0.000  
Primary Var: S, Mises  
Deformed Var: U Deformation Scale Factor: +1.000e+00

# Constitutive models

- (Linear) Hookean:

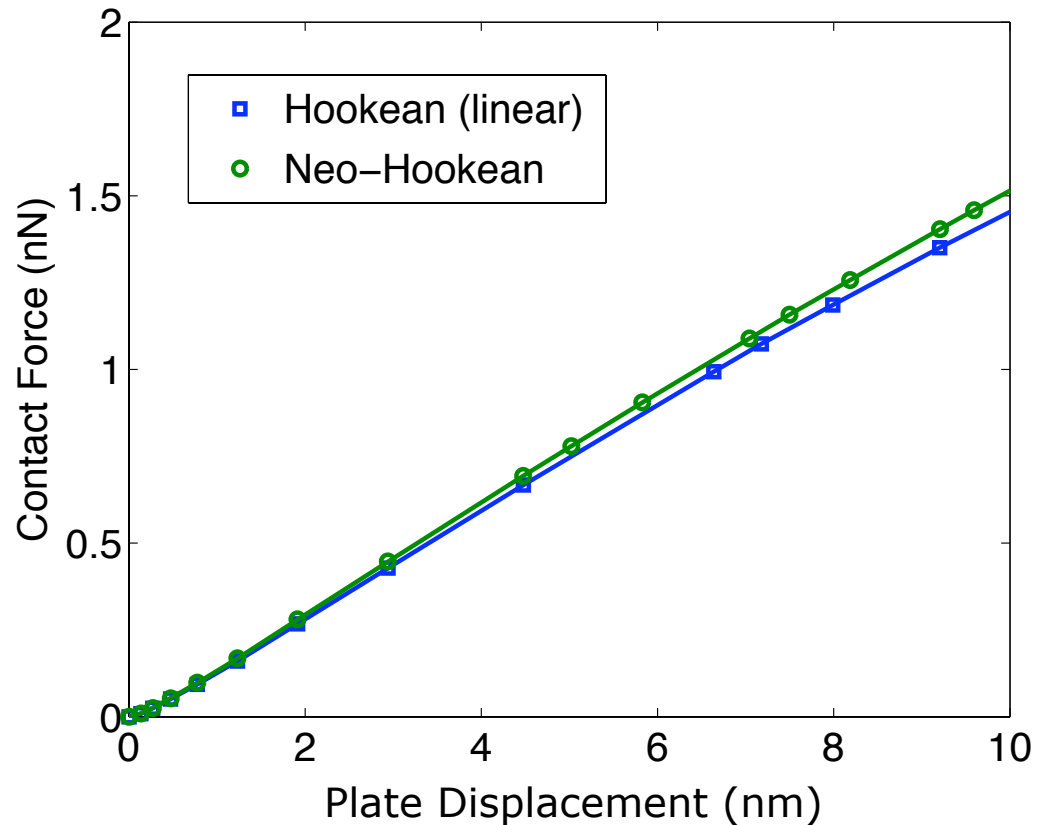
$$w = \frac{\lambda}{2} (\text{tr } \mathbf{E})^2 + \mu (\text{tr } \mathbf{E}^2)$$

$$\boldsymbol{\sigma} = \lambda (\text{tr } \mathbf{E}) \mathbf{1} + 2\mu \mathbf{E}$$

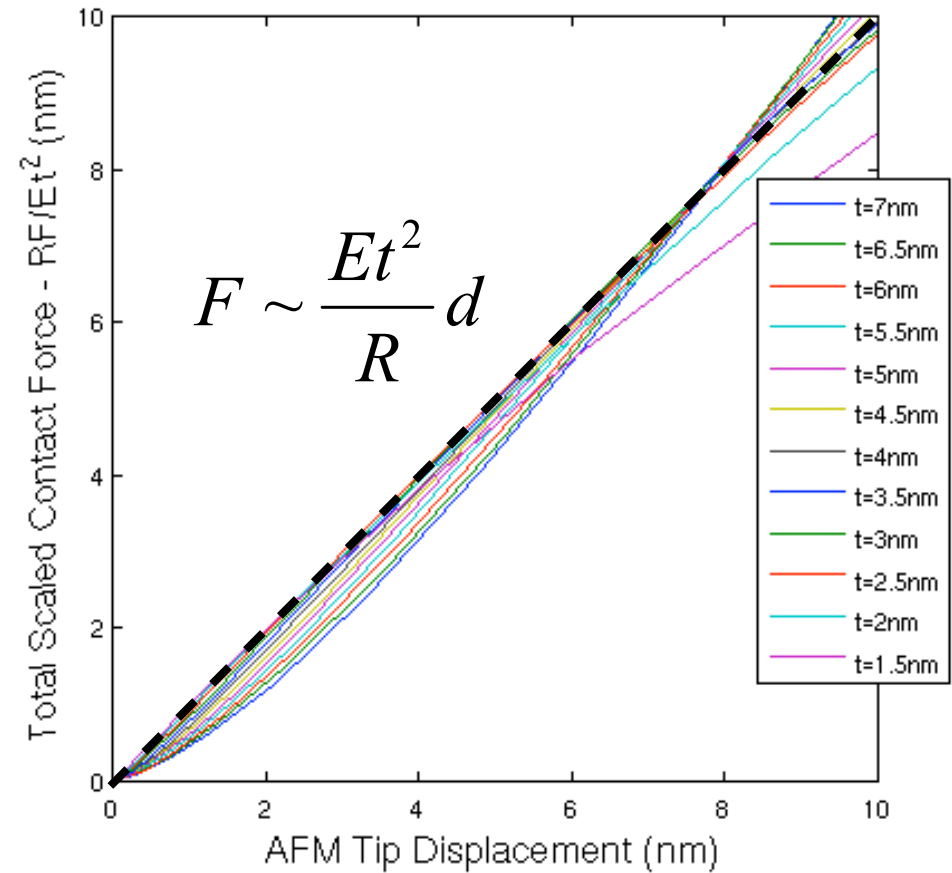
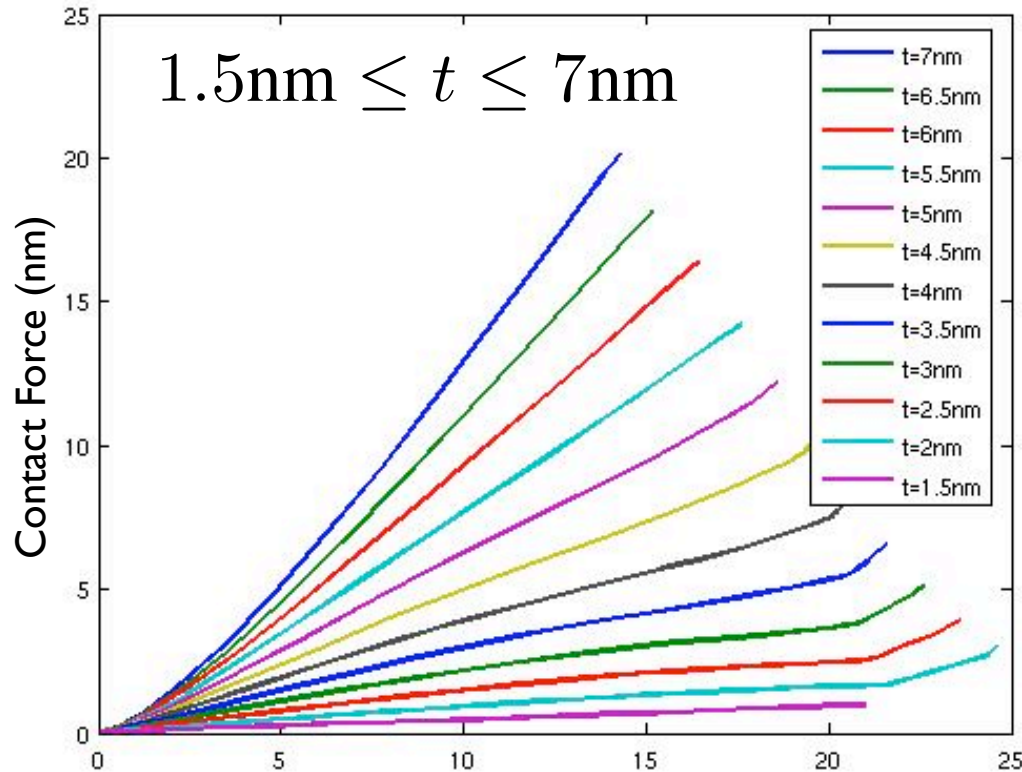
- Compressible Neo-Hookean (rubber elasticity):

$$w = \frac{1}{2} \lambda_0 (\ln J)^2 - \mu_0 \ln J + \frac{\mu_0}{2} (\text{tr } \mathbf{C} - 3)$$

$$\mathbf{C} = 2\mathbf{E} + \mathbf{1} \quad J = (\det \mathbf{C})^{1/2}$$



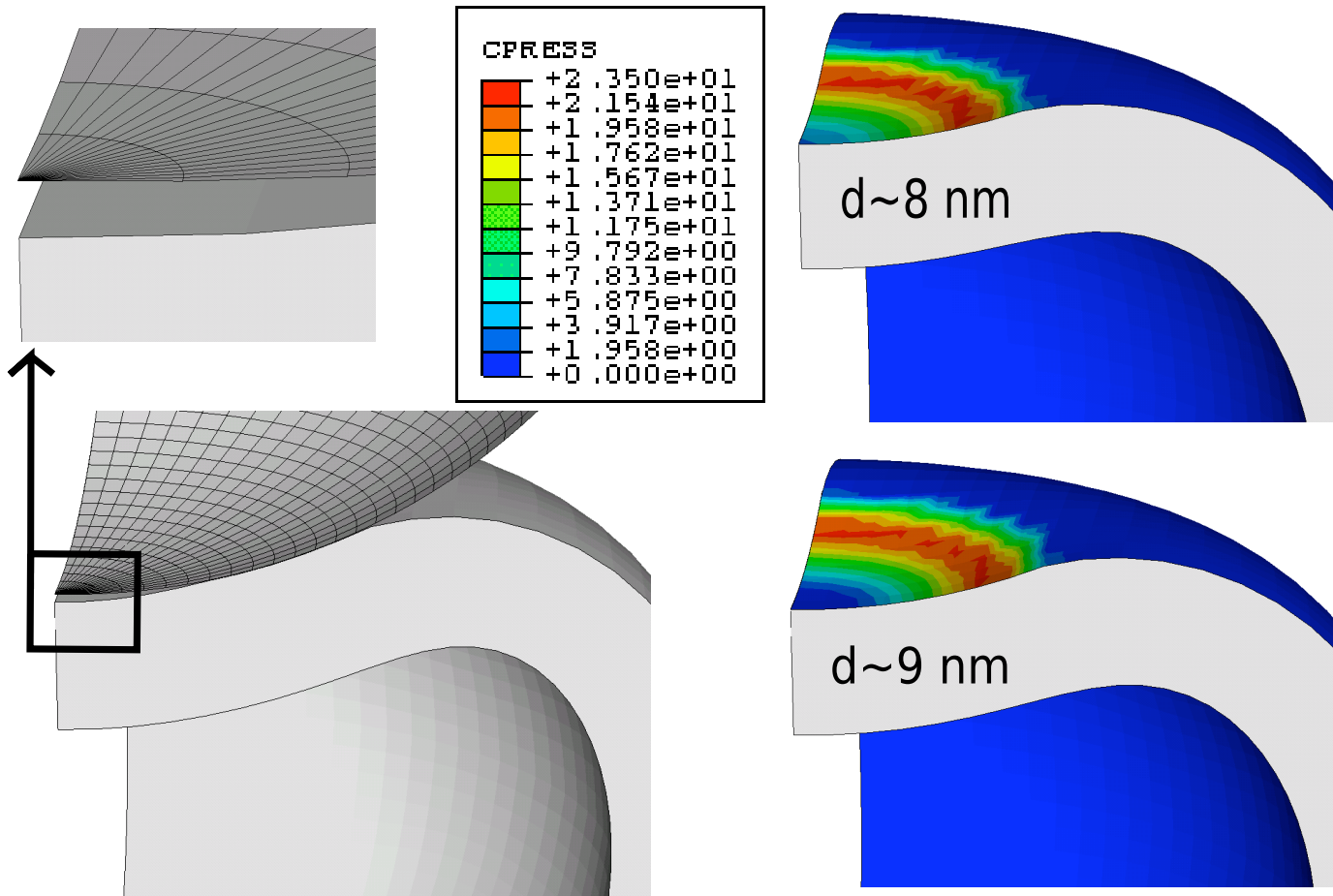
# Thickness Variation



“Most” linear at  $t \approx 3\text{nm}$  (average physical thickness)

Fit to experiment:  $E \approx 250\text{MPa}$

# “Buckling”-type separation from tip

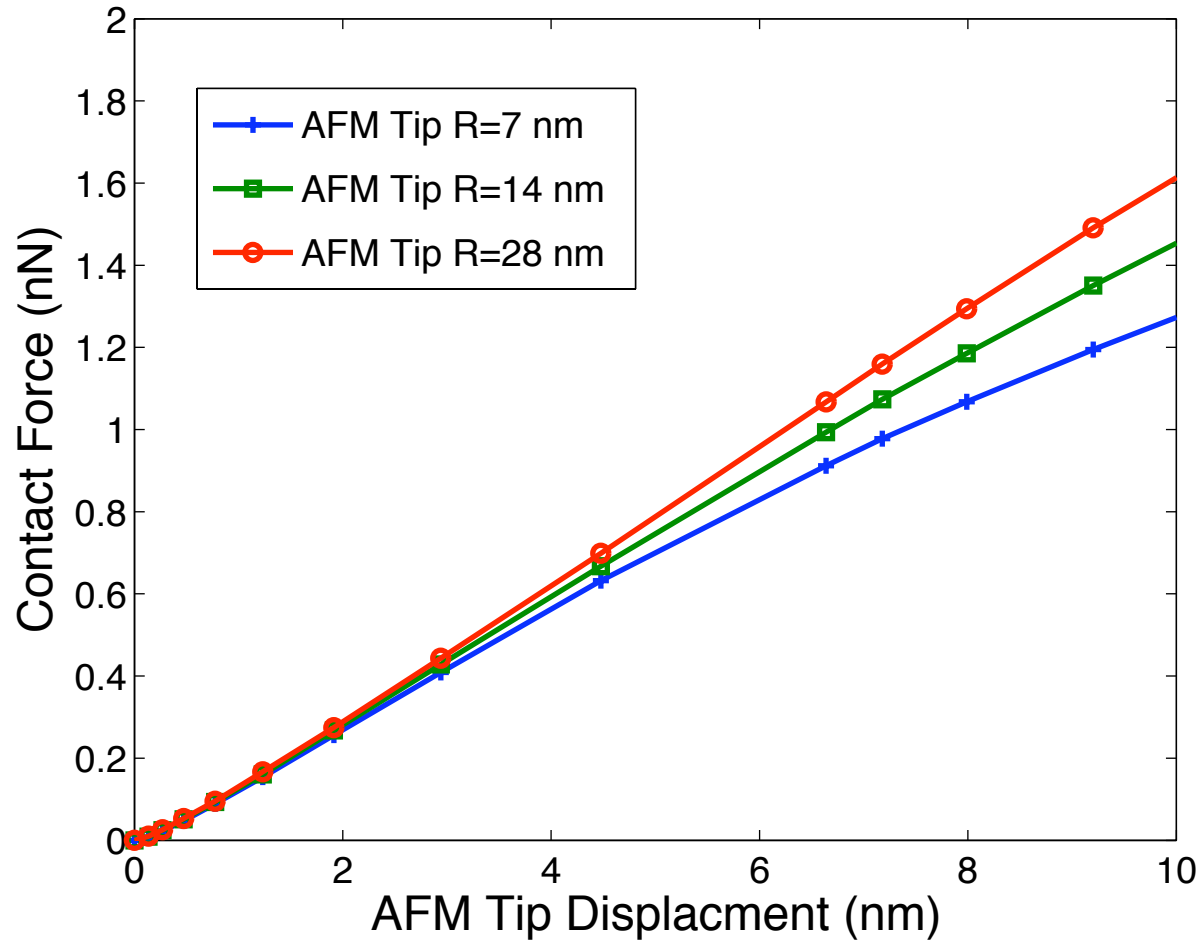


(a) Capsid Buckling,  $d \sim 12$  nm

(b) Contact Pressure

Separation is associated with a softening of force response

# Inensitivity to Tip-size



# Lessons from 3-D models

- Thickness affects linearity
- Results insensitive to tip size, constitutive model
- Signs of buckling observed
- No explanation of failure



# 2-D Continuum Model: Thin Icosahedral Shell

considering structural symmetries

- Lidmar, Mirny, Nelson, PRE (2003)

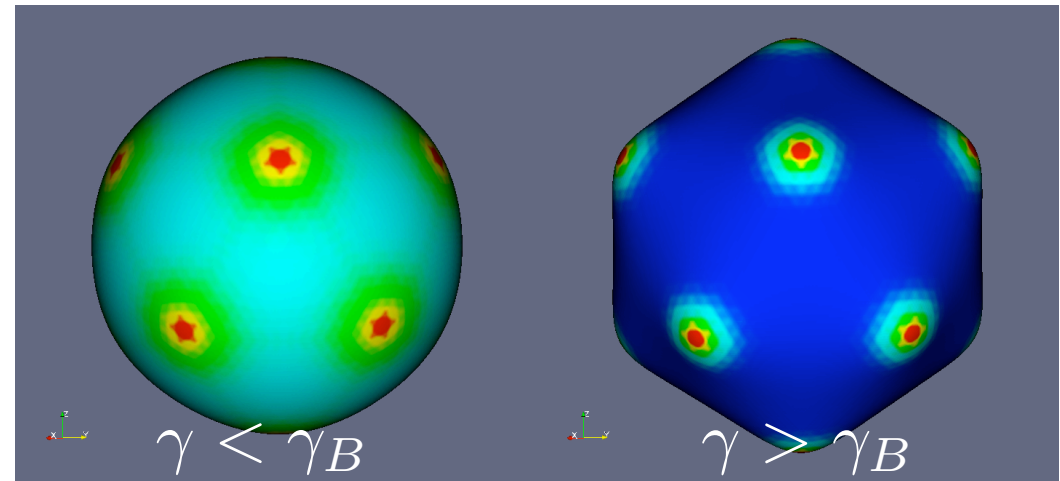
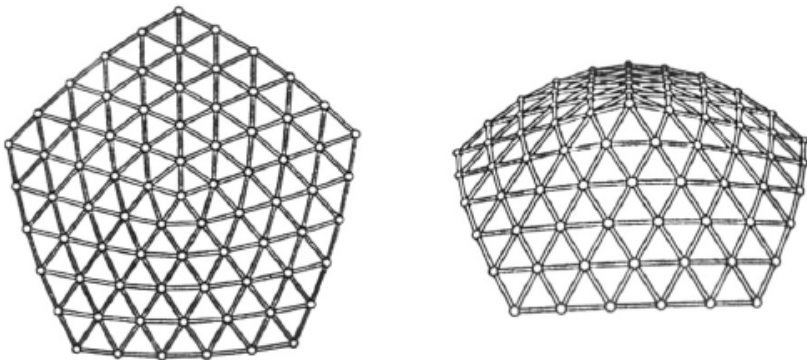
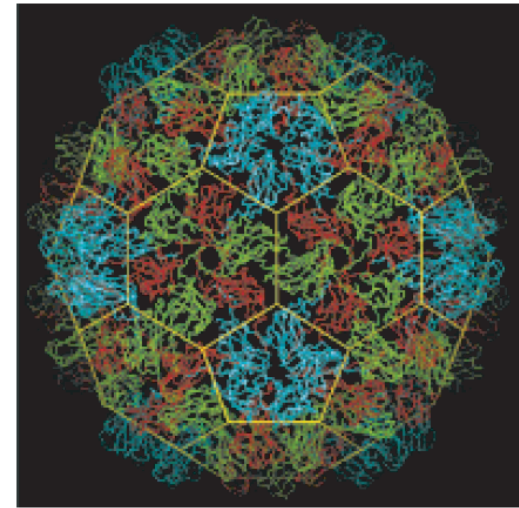
- Energy is a balance of bending and stretching

$$\mathcal{H} = \frac{\kappa}{2} \int H^2 dA + \frac{1}{2} \int (\lambda E_{ii}^2 + 2\mu E_{ij} E_{ij}) dA - W^{\text{ext}}$$

- Faceting controlled by Föppl - von Kármán number

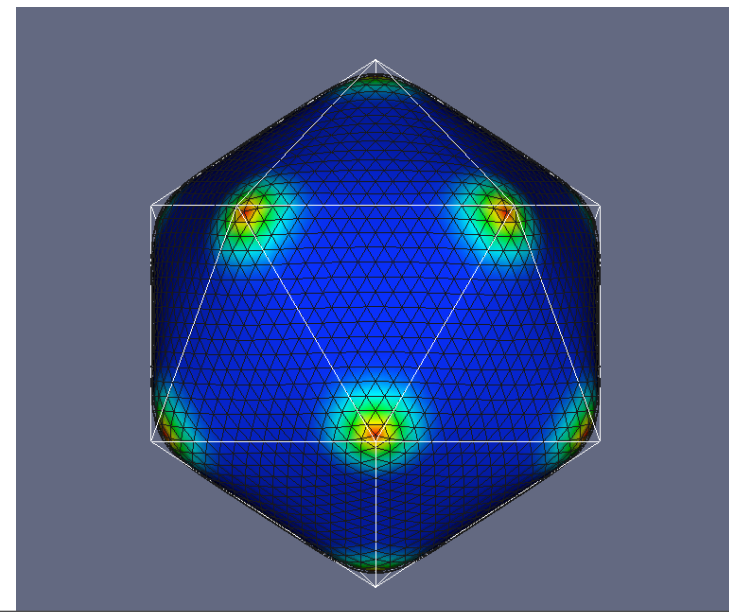
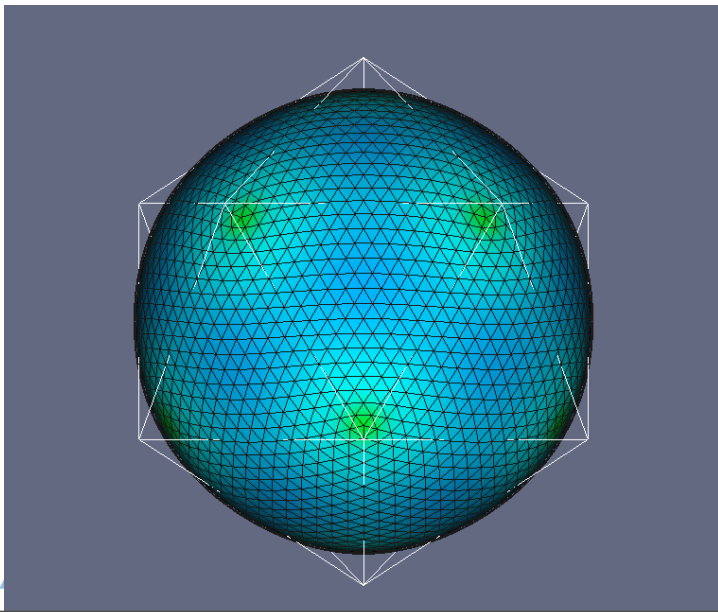
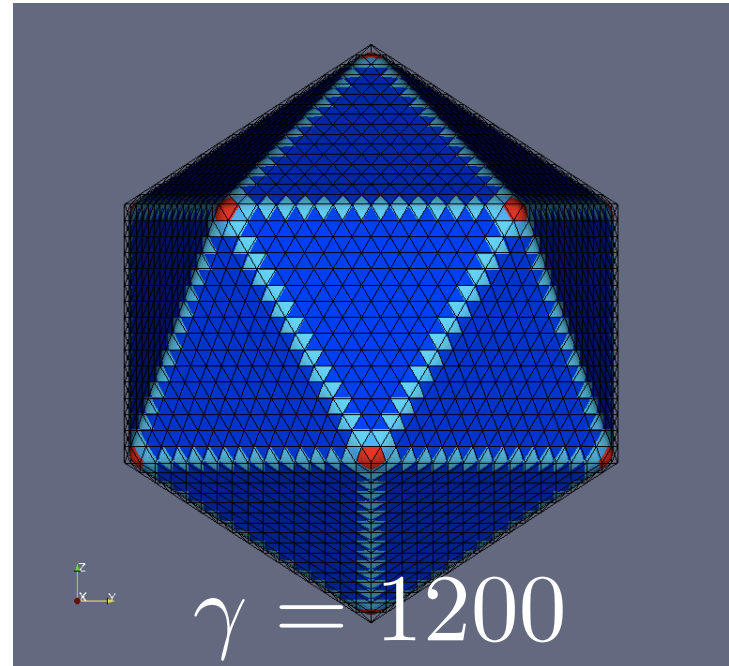
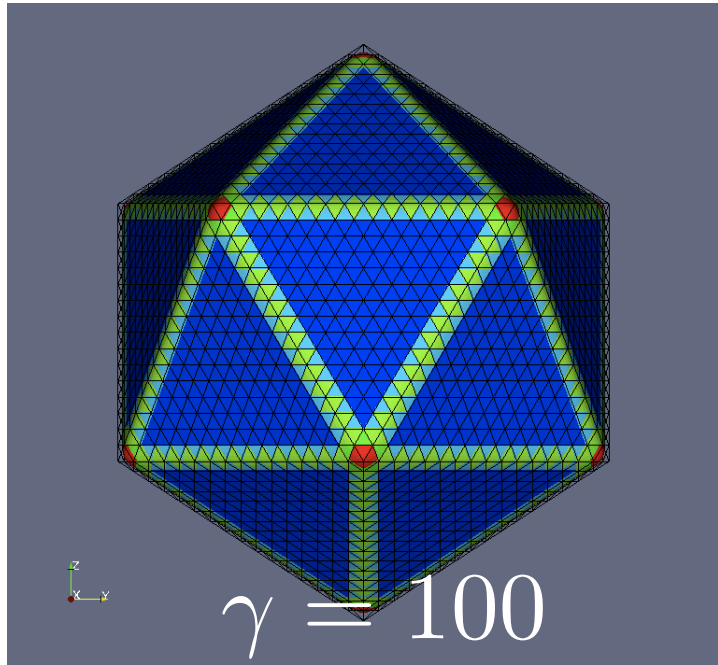
$$\gamma = \frac{Y R^2}{\kappa} \quad Y = \frac{4\mu(\mu + \lambda)}{2\mu + \lambda}$$

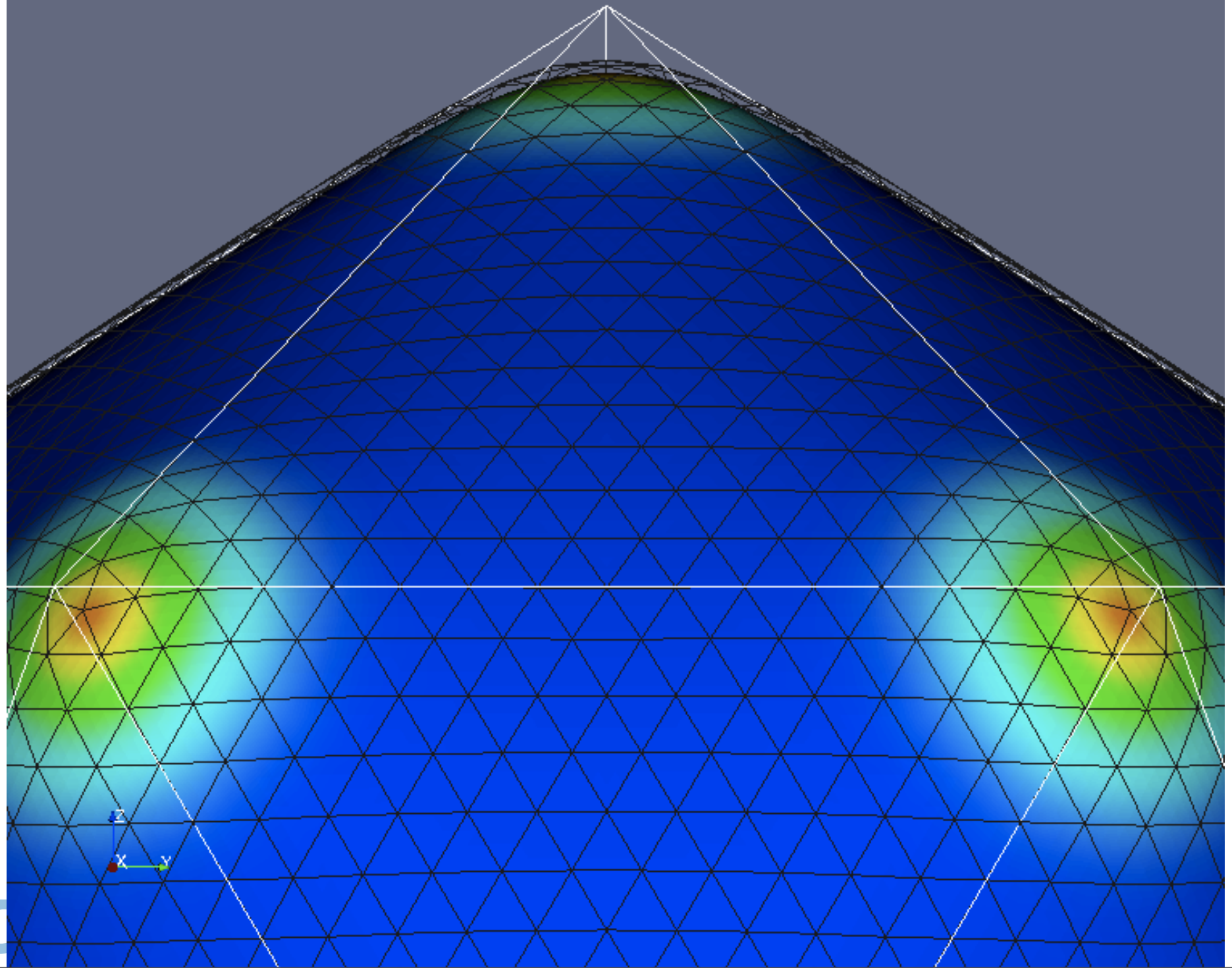
- 5-fold sites are Disclinations



# Thin-shell Finite Elements

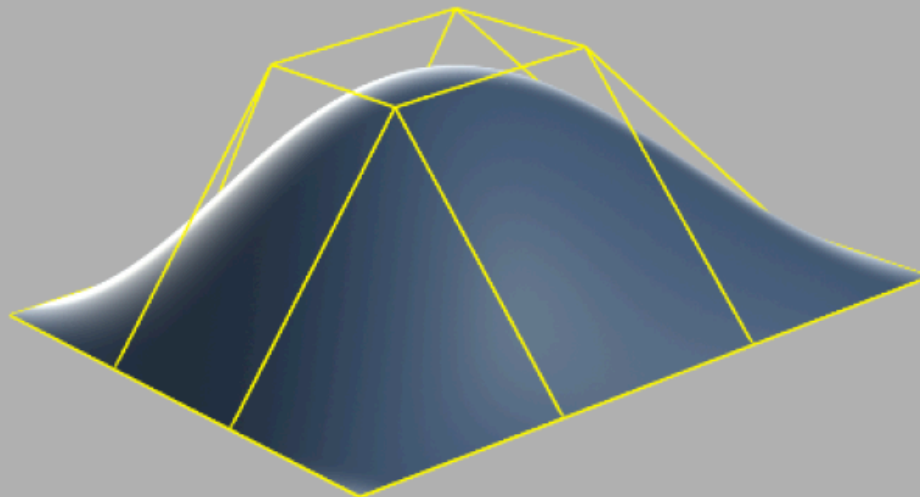
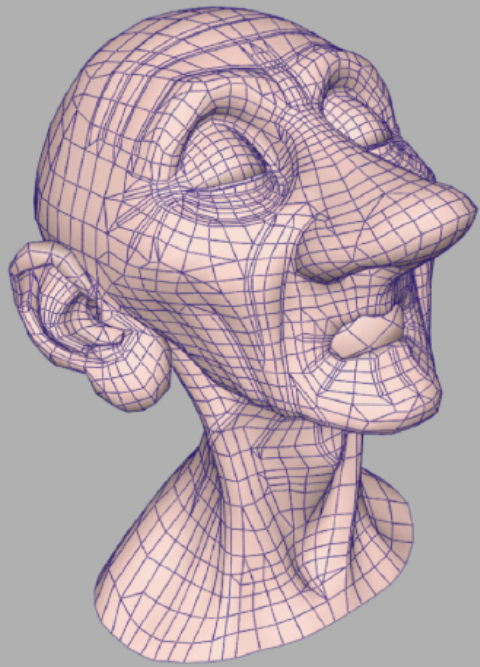
2562 vertex (T=256) mesh







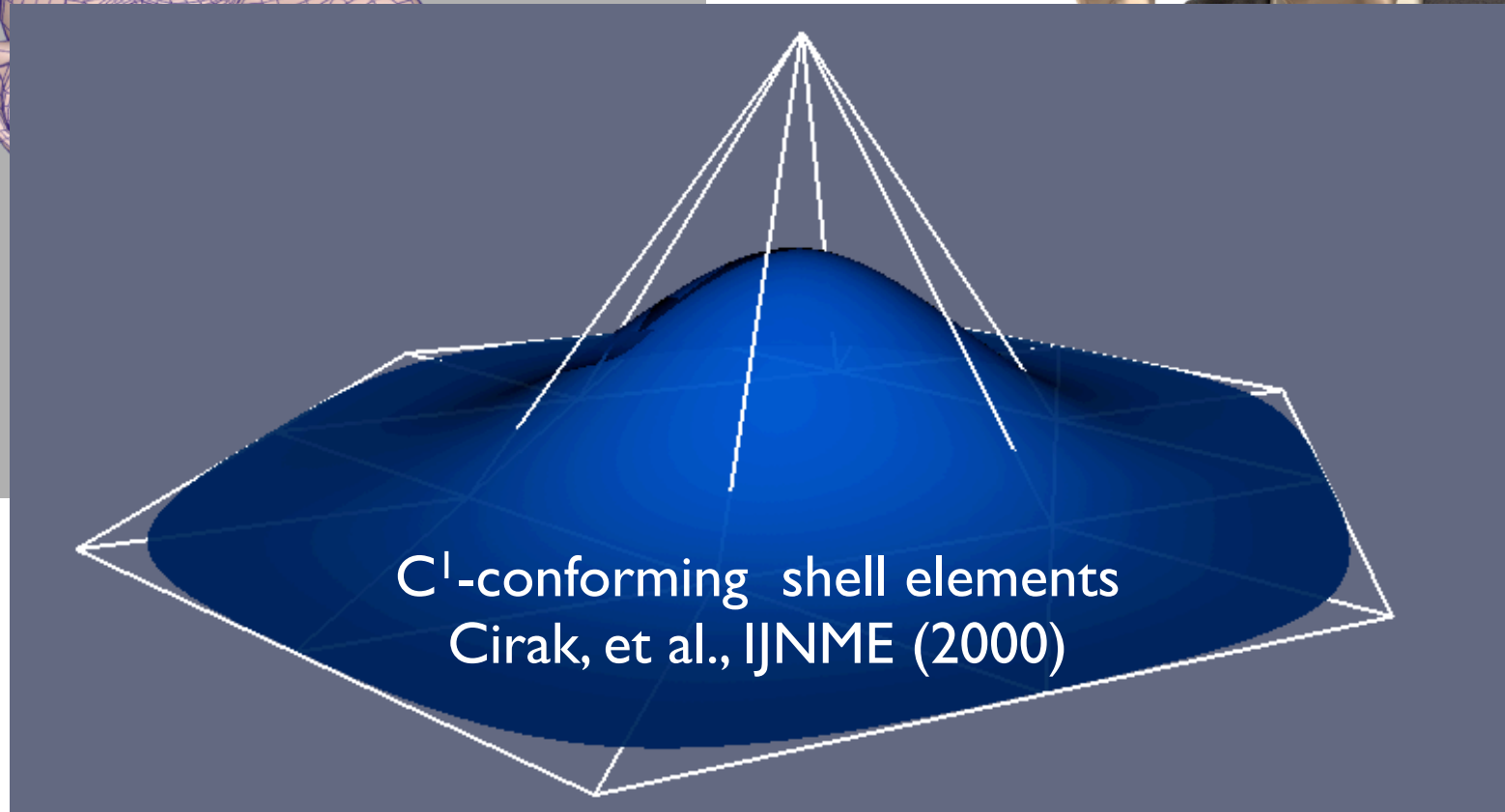
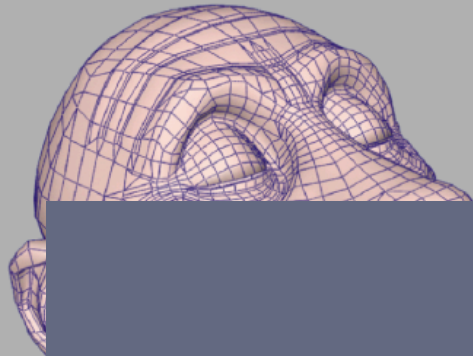
# Local Polynomial Approximation



UCLA

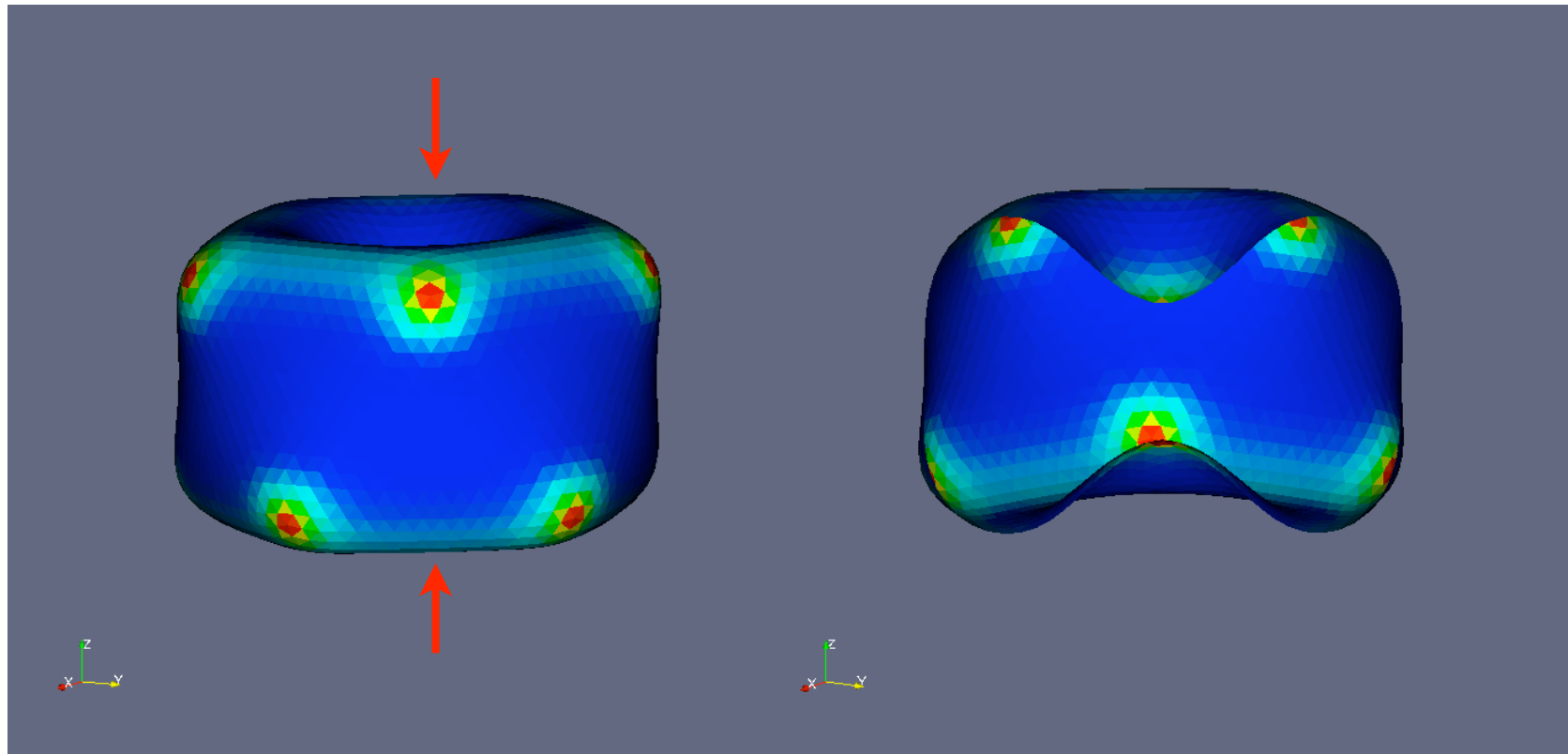
Pixar Studios *Geris Game*

# Local Polynomial Approximation



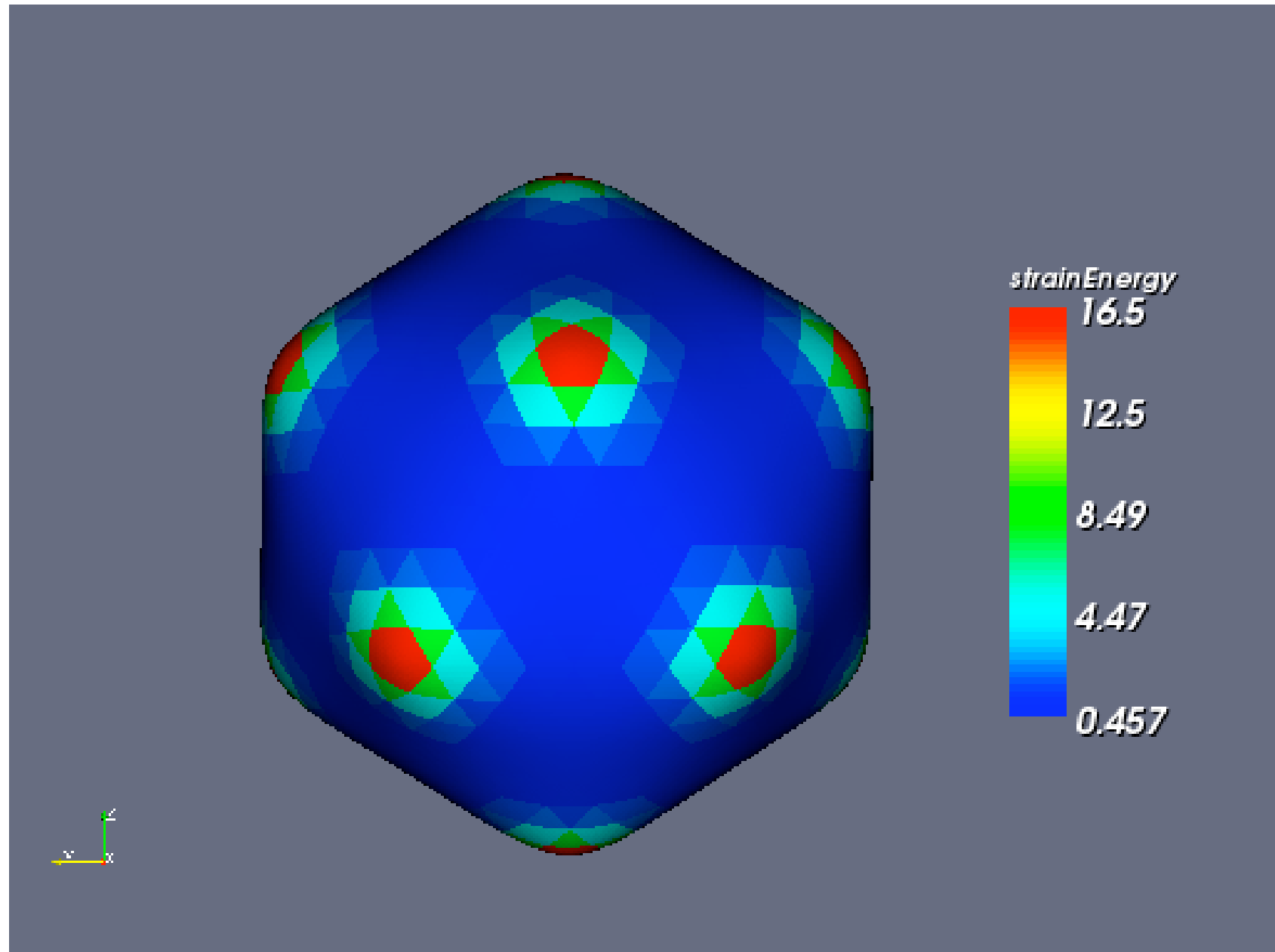
$C^1$ -conforming shell elements  
Cirak, et al., IJNME (2000)

# Icosahedral imperfections facilitate Buckling



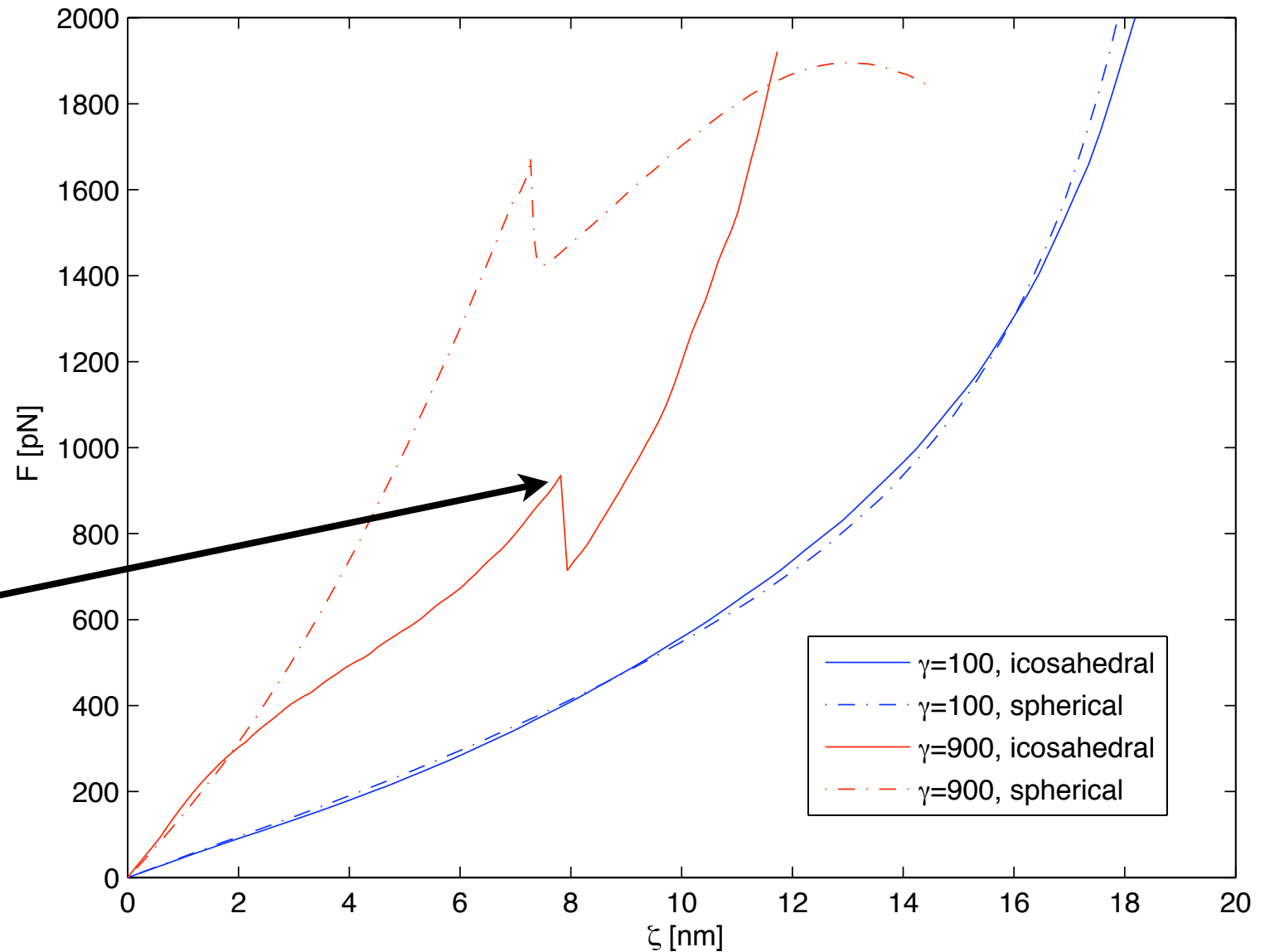
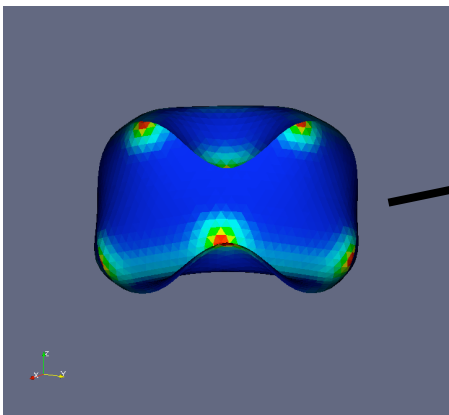


# Icosahedral imperfections facilitate Buckling



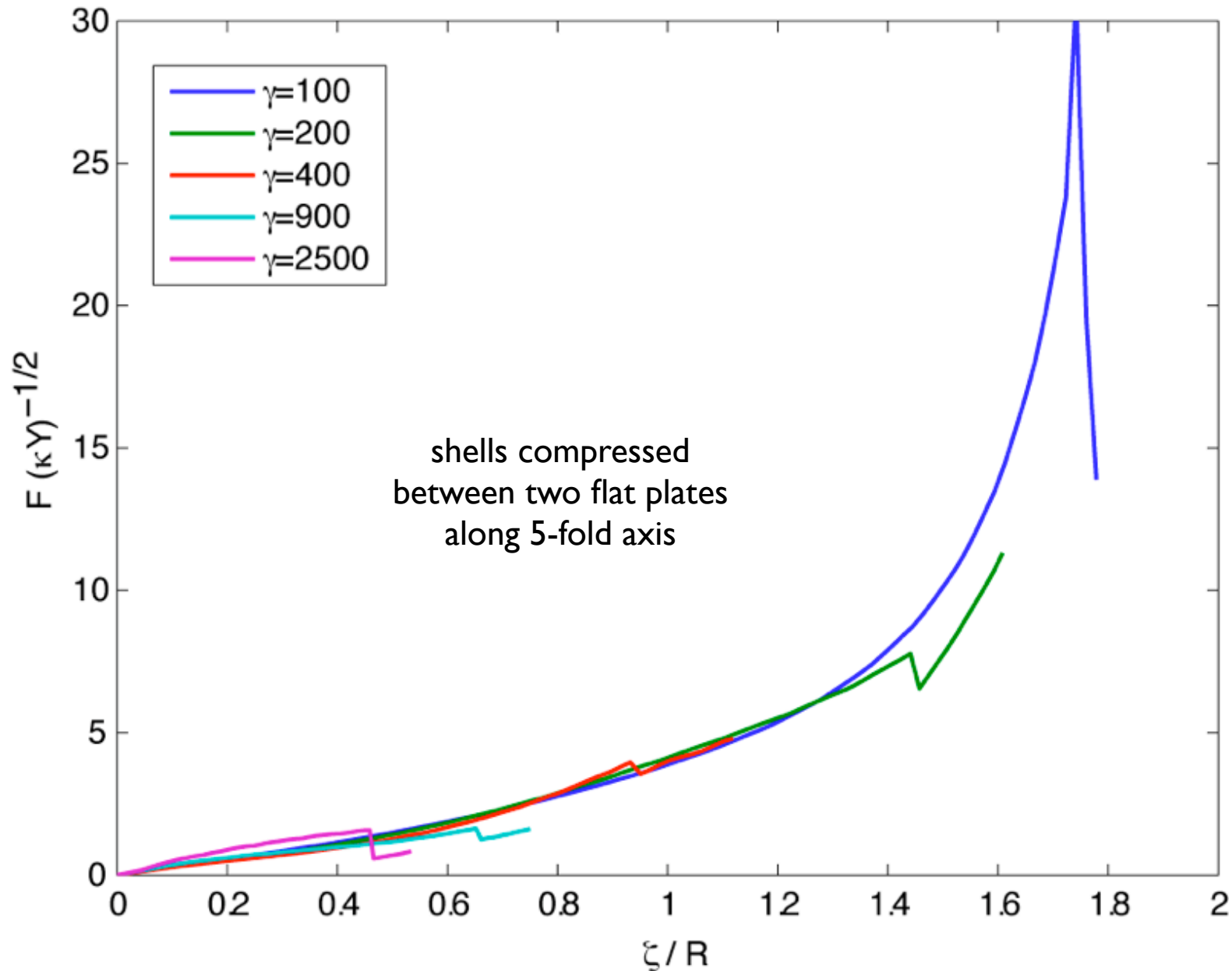
# Icosahedral imperfections facilitate Buckling

shells compressed  
between two flat plates  
along 5-fold axis

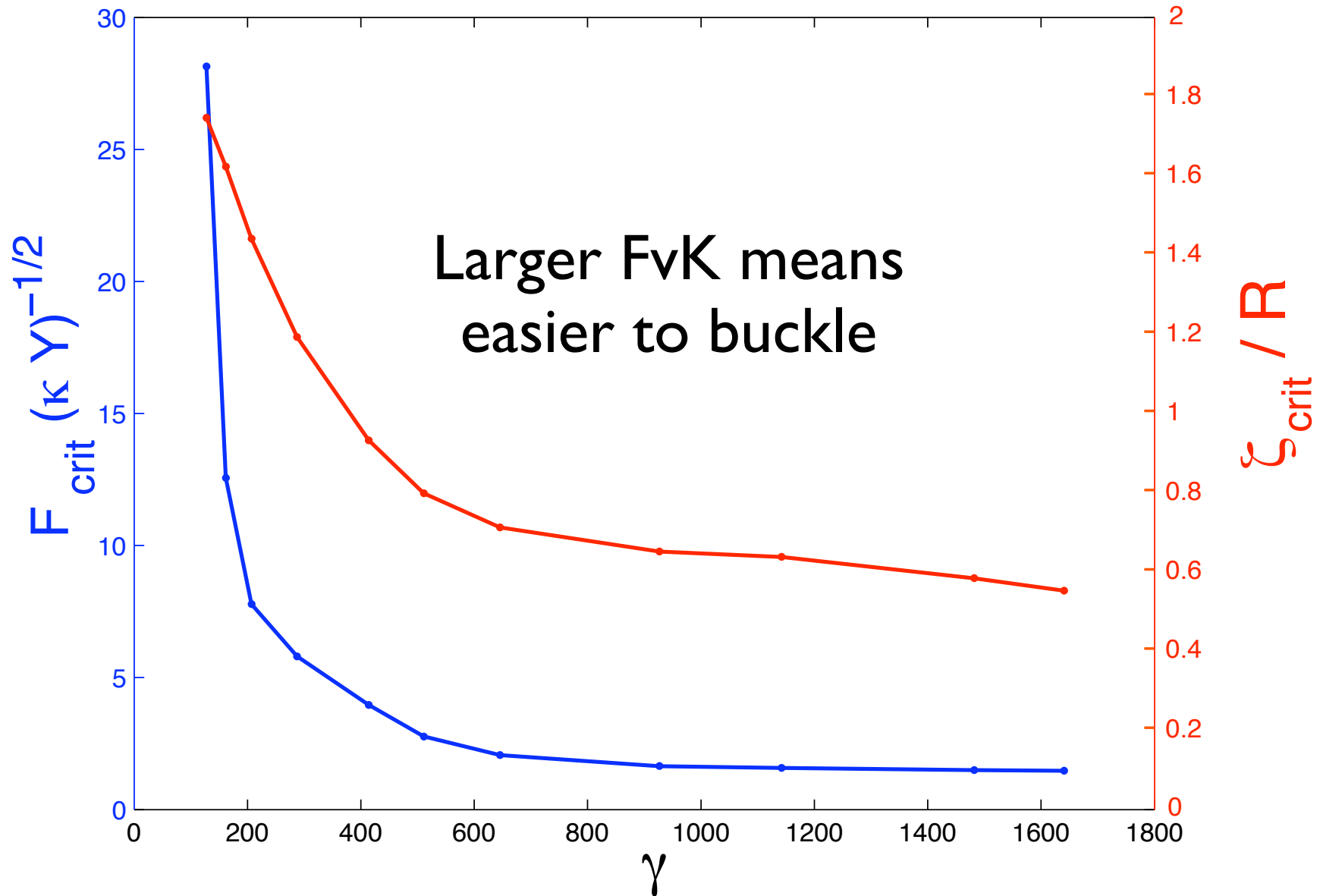


Dashed lines: ref. state is spherical

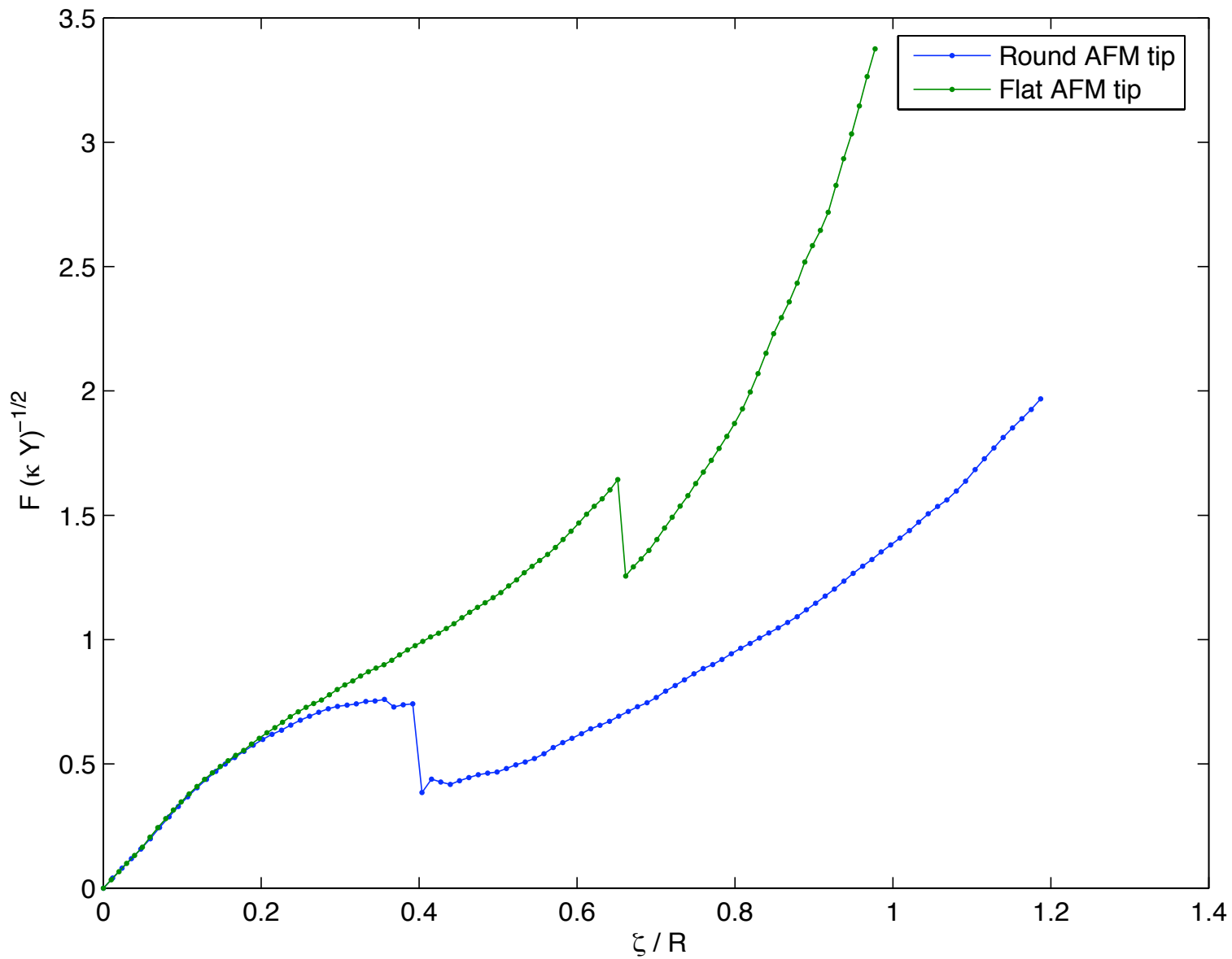
# Scaled Force-deflection response vs FvK number



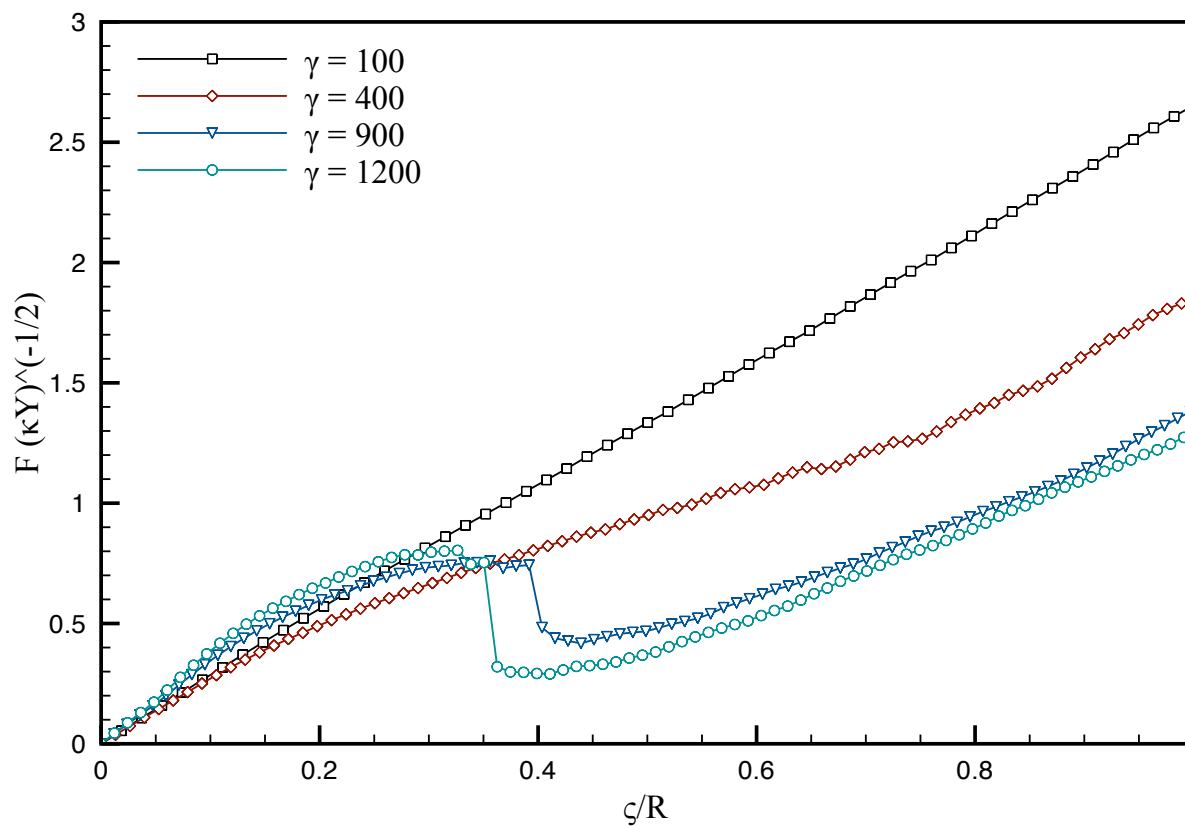
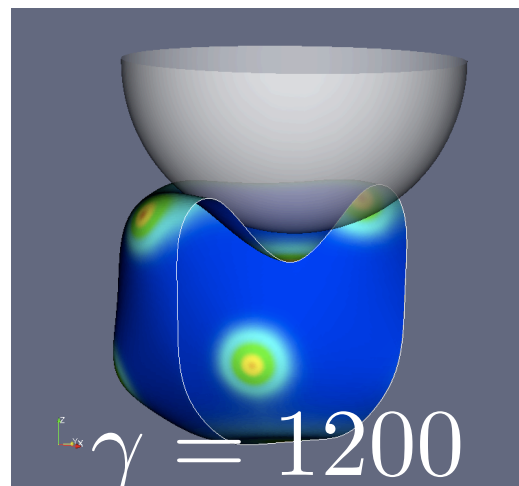
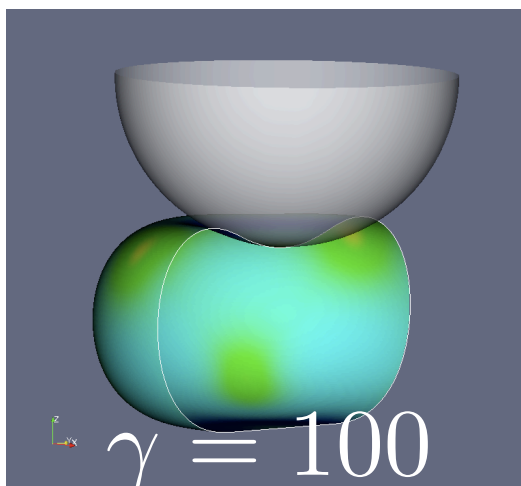
# Critical force and deflection vs FvK number



# Influence of Tip Shape

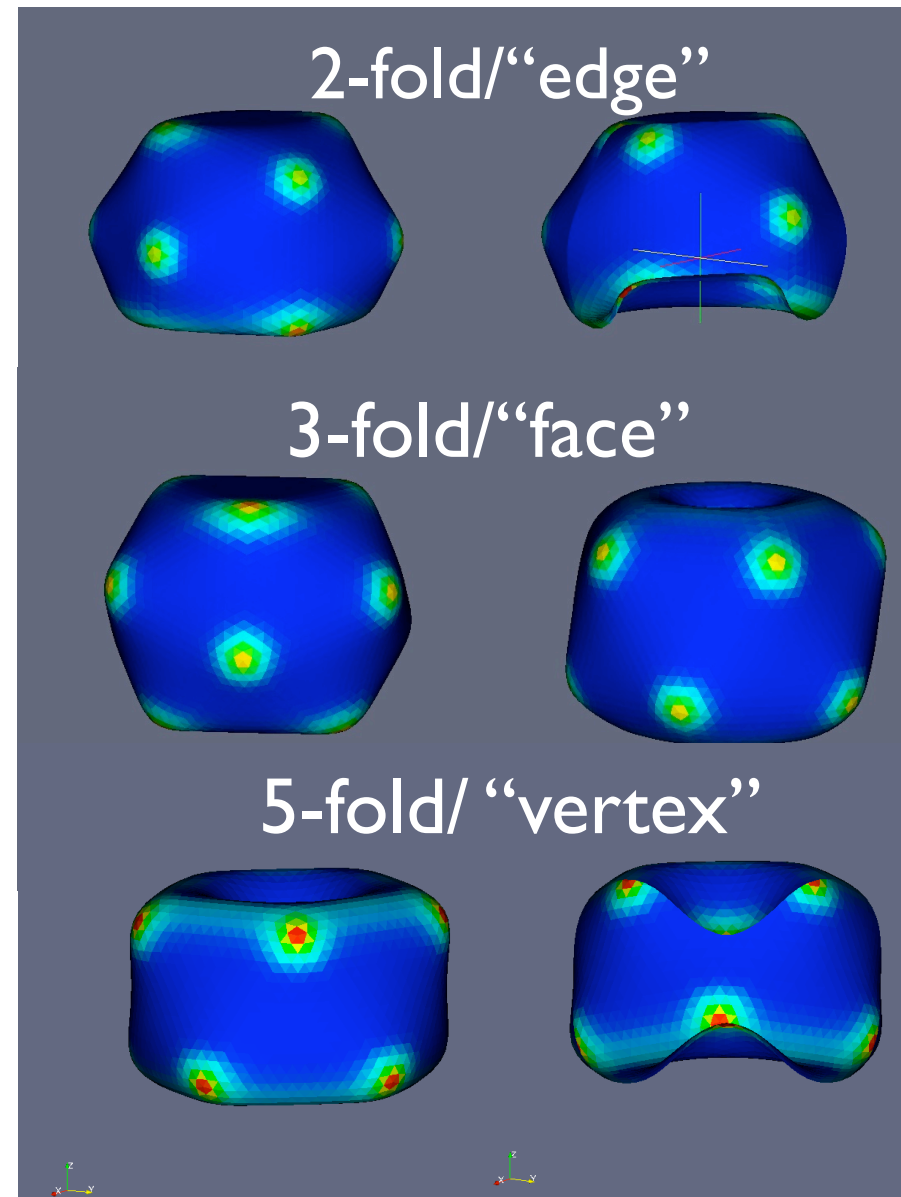
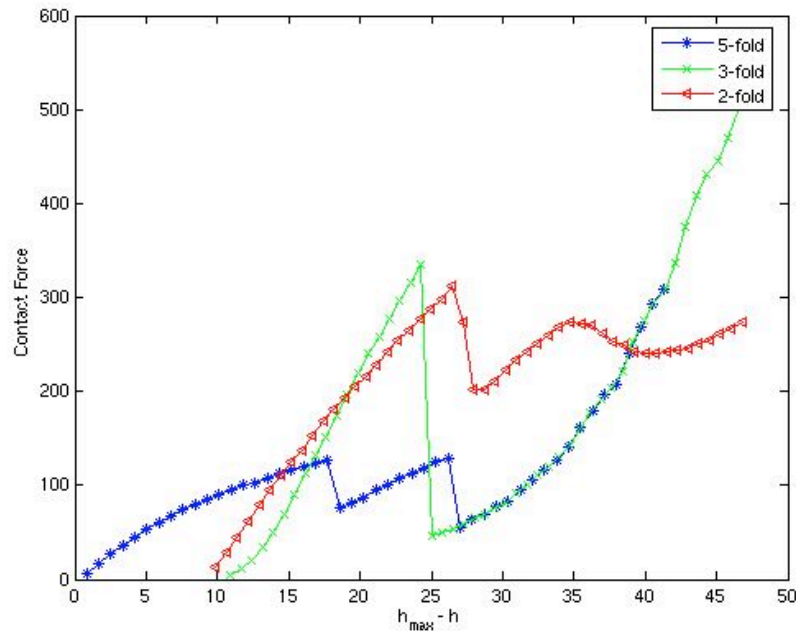
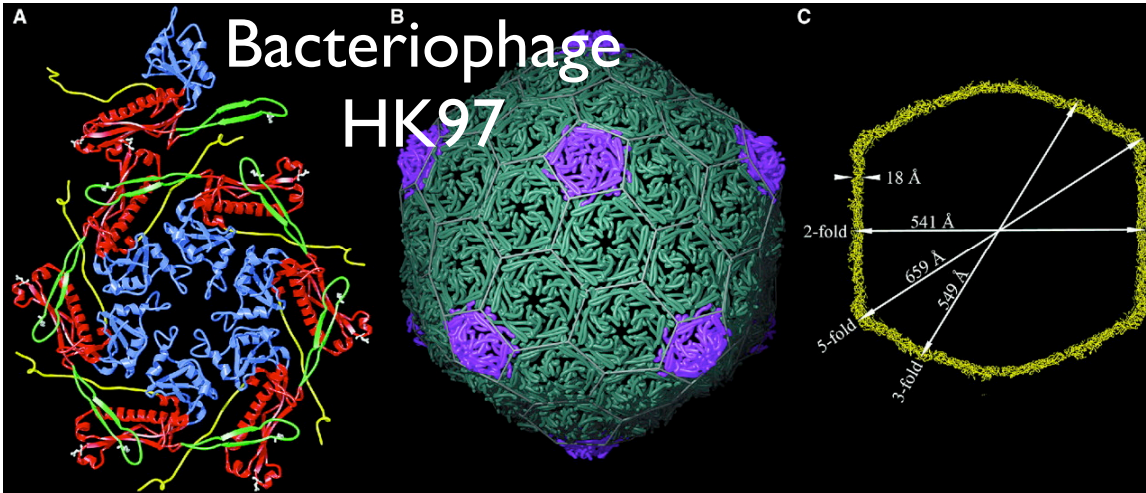


# Simulating AFM experiments

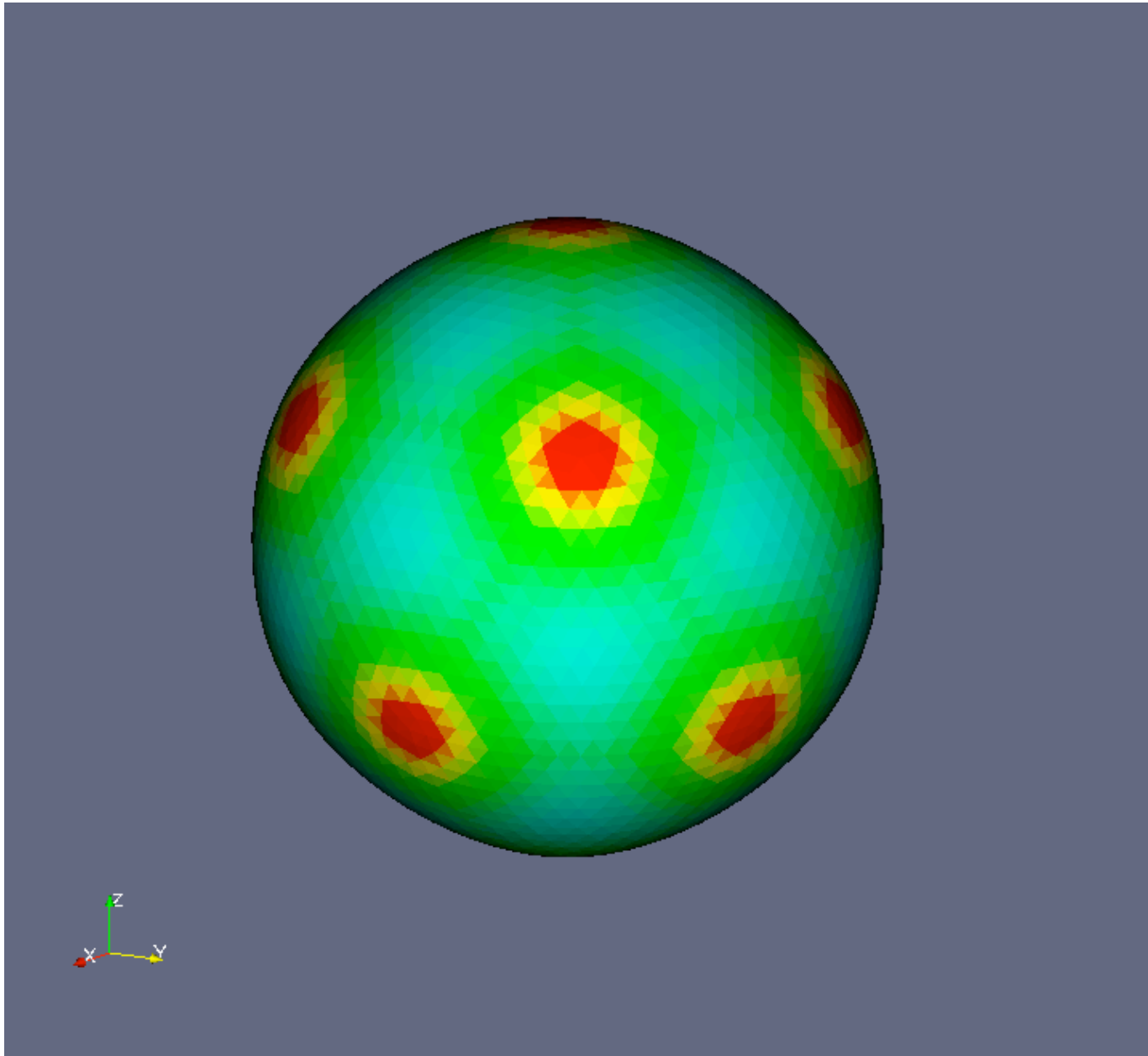




# Orientation Dependence



# A small virus free to rotate

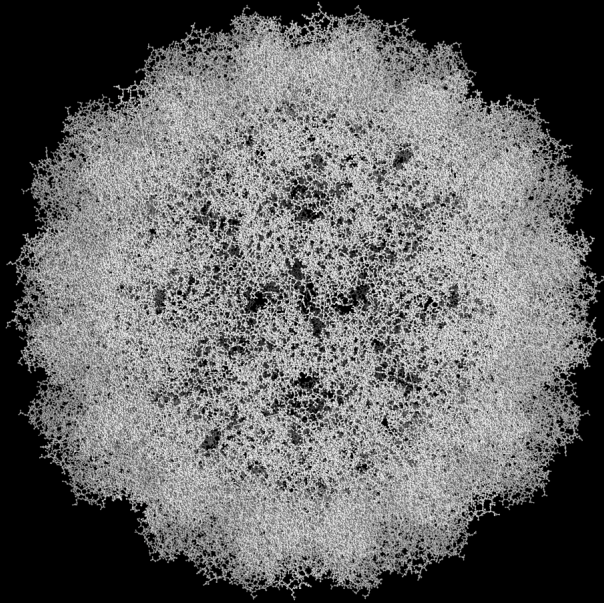


# Lessons from 2-D models

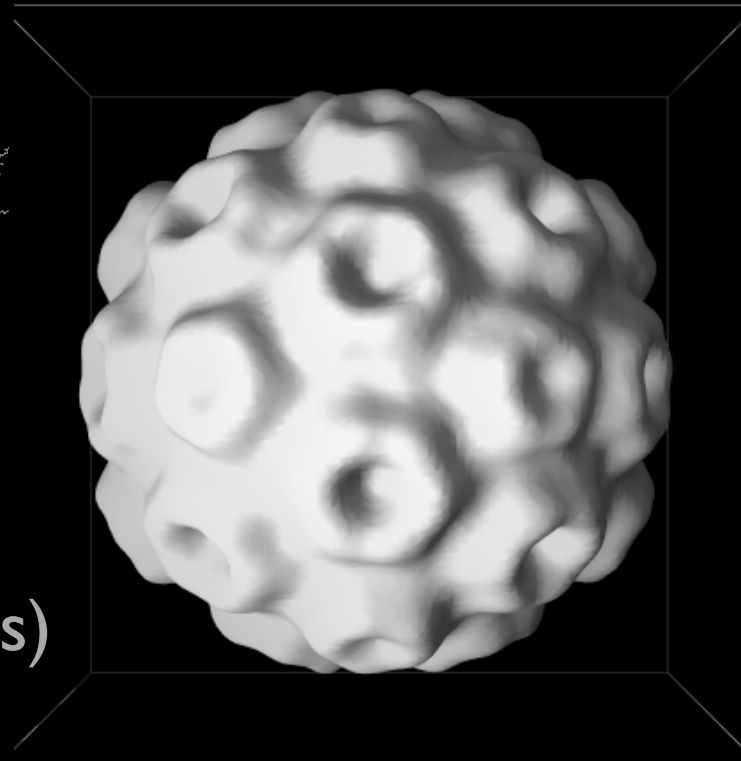
- 5-fold sites can act like structural imperfections, triggering instabilities
- Critical force/displacement varies with  $FvK$
- Orientation stability varies with  $FvK$

# Strategy for multi-scale modeling

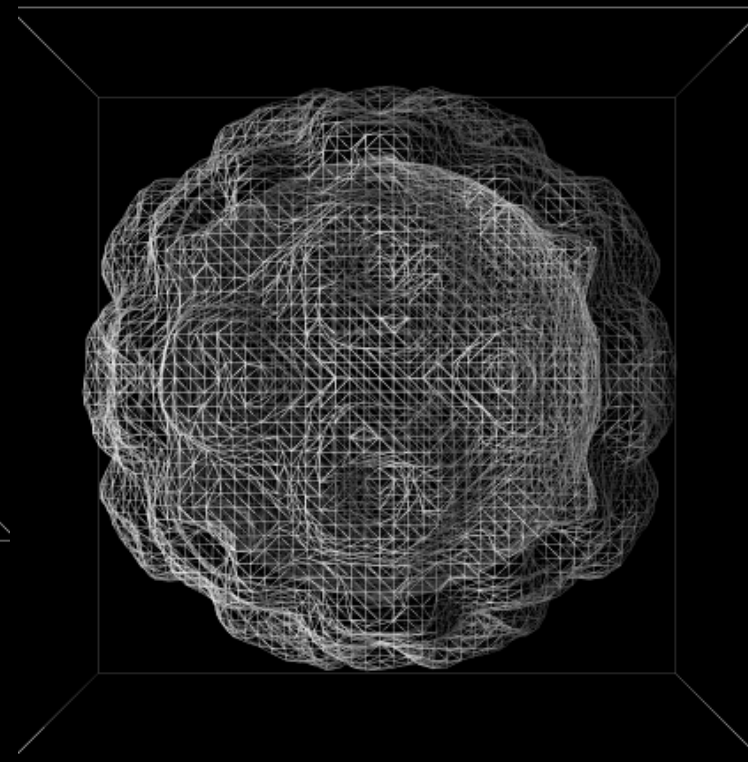
# Strategy for multi-scale modeling



High resolution  
(atomic coordinates)



Low resolution  
(cryo-EM-like density)



Finite Element mesh

# Acknowledgements

- Melissa Gibbons (UCLA MAE): FE modeling of viruses.
- Chuck Knobler, Bill Gelbart, Jean-Philippe Michel (UCLA Chemistry): AFM nanoindentation experiments on CCMV.
- Robijn Bruinsma (UCLA Physics): Capsid buckling.